



# Avery I and II

Transportation Impact Analysis

# Tualatin, Oregon

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### **Executive Summary**

- 1. The proposed development at 10500/10700 SW Tualatin-Sherwood Road includes the construction of two industrial buildings totaling approximately 112,500 square feet. Construction is expected to be completed with occupancy beginning in the year 2023.
- 2. The proposed development is estimated to generate 83 morning peak hour, 73 evening peak hour, and 548 average weekday trips.
- 3. Based on a review of the available crash data and crash rates, patterns are consistent with the geometry and traffic control provided at the study intersection. The proposed project is not expected to change or worsen crash rates. Accordingly, no safety mitigation is recommended per the crash data analysis.
- 4. Preliminary traffic signal warrants are not met at any of the unsignalized study area intersections under buildout conditions.
- 5. The study intersection is currently operating acceptably per Washington County standards and is projected to continue operating acceptably through the 2023 buildout year of the site. No operational mitigation is required or recommended.
- 6. The construction of the planned five lane cross-section on SW Tualatin-Sherwood Road will not adversely affect future operations at the study intersection.



### Introduction

The proposed development at 10500/10700 SW Tualatin-Sherwood Road includes the construction of two industrial buildings totaling approximately 112,500 square feet. Construction is expected to be completed with occupancy beginning in the year 2023.

Based on correspondence with the City of Tualatin staff, the study area includes one intersection:

• Site Access at SW Tualatin-Sherwood Road

This report examines the impacts of the proposed development on the transportation system in the vicinity of the project site. The purpose of this study is to analyze potential traffic impacts and recommend any required transportation mitigation measures to ensure safe and efficient performance of the transportation facilities that will be impacted by the proposed development. In addition to the operational analysis, the report includes a safety analysis at the study intersection.

Detailed information on traffic counts, trip generation calculations, safety analyses, and operations are included in the appendices to this report.

### Location Description

The project site is located south of SW Tualatin-Sherwood Road, north of SW Avery Street, and west of SW Teton Avenue in Tualatin, Oregon. The proposed development includes the construction of two warehouse buildings totaling approximately 112,525 square feet on two tax lots (tax lots 2S126B00105 and 2S127AA02100). Both parcels are zoned General Manufacturing (MG) and are centrally located within Tualatin's industrially zoned lands.

The Avery I site is located at 10700 SW Tualatin-Sherwood Road and will house an 81,075 square-foot warehouse. The Avery II site is located at 10500 SW Tualatin-Sherwood Road and will house a 31,050 square-foot warehouse. Both sites will take access from SW Tualatin-Sherwood Road via an existing shared driveway.

An aerial view of the proposed site and the nearby vicinity is displayed in Figure 1, with the subject sites outlined in yellow. A site plan is included in Appendix A.





Figure 1: Project Location (image from Google Maps)

### Vicinity Roadways

The proposed development is expected to impact two major roadways near the site. Table 1 provides a description of each of the vicinity roadways.

Table 1: Vicinity Roadway Descriptions

| Roadway                       | Classification    | Jurisdiction         | Travel<br>Lanes | Speed<br>(mph) | Curbs         | Sidewalks                                | Bicycle<br>Lanes | On-Street<br>Parking |
|-------------------------------|-------------------|----------------------|-----------------|----------------|---------------|--|------------------|----------------------|
| SW Tualatin-<br>Sherwood Road | Major<br>Arterial | Washington<br>County | 3-5             | 45<br>(Posted) | Both<br>Sides | Both Sides                               | Both<br>Sides    | Not<br>Permitted     |
| SW Teton<br>Avenue            | Minor<br>Arterial | City of<br>Tualatin  | 3               | 35<br>(Posted) | Both<br>Sides | Both Sides w/<br>Exceptions <sup>1</sup> | None             | Not<br>Permitted     |

Notes:

1. Sidewalk is missing on west side of SW Teton Avenue where adjacent land is undeveloped between SW Tualatin-Sherwood Road and SW Manhasset Drive.



### Study Intersections

Through coordination with the City of Tualatin and Washington County, one study intersection was identified for analysis. A summarized description of the study intersection is provided in Table 2.

| Table 2 | 2: Study | Intersection | Descriptions |
|---------|----------|--------------|--------------|
|---------|----------|--------------|--------------|

| Intersection |  | Geometry     | Traffic Control | Phasing/Stopped Approaches |
|--------------|--|--------------|-----------------|----------------------------|
| 1            | Site Access (Existing) at<br>SW Tualatin-Sherwood Road | Three-Legged | Stop-Controlled | NB Stop-Controlled         |

### Public Transit

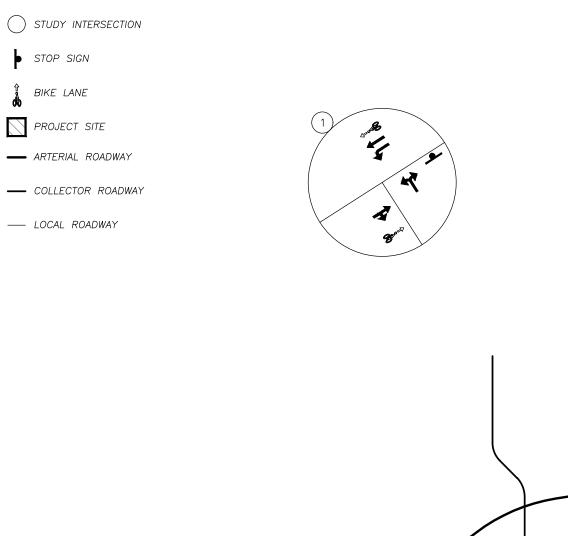
The project is located near one transit line that has stops within an approximate one-half mile walking/biking distance from the site.

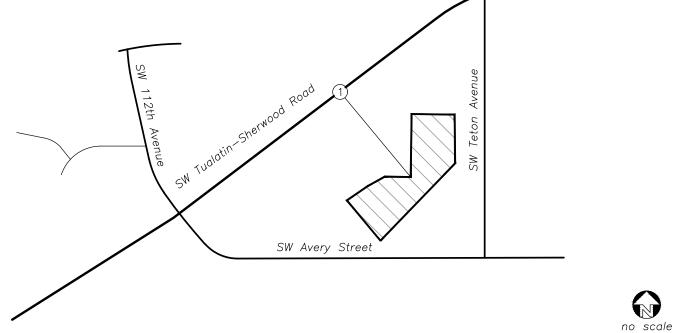
Bus Line # 97 – *Tualatin-Sherwood Road* provides weekday rush-hour service between W Langer Drive/Sherwood Plaza and the Tualatin WES Station. The nearest bus stops to the site are located at the intersection of SW Teton Avenue and SW Tualatin-Sherwood Road. Weekday service is scheduled with four westbound and three eastbound trips in the morning at approximately 60-minute headways. Afternoon service is scheduled with four eastbound and three westbound trips at approximately 60-minute headways. There is currently no weekend or holiday service.

A vicinity map showing the project site, vicinity streets, and study intersection configuration is shown in Figure 2.











VICINITY MAP

Figure 2 Avery | & || 2/8/2022

## Site Trips

### Trip Generation

To estimate trips that will be generated by the proposed development, trip rates from the *Trip Generation Manual*<sup>1</sup> were used. Based on direction from City of Tualatin staff, data from land-use code 110 (*General Light Industrial*) was used to estimate the proposed development's trip generation based on square footage of gross floor area. The client has indicated that both buildings in the proposed development will be used for the storage and distribution of materials.

The trip generation calculations show that the proposed development is projected to generate 83 trips during the morning peak hour, 73 trips during the evening peak hour, and 548 trips during the average weekday. The trip generation estimates are summarized in Table 3. Detailed trip generation calculations are included in Appendix A.

#### Table 3: Trip Generation Summary

| Land Use                 | ITE<br>Code | Size/Rate | Morning Peak Hour |     |       | Eveni | ng Peak | Weekday<br>Total |     |
|--------------------------|-------------|-----------|-------------------|-----|-------|-------|---------|------------------|-----|
|                          |             |           | In                | Out | Total | In    | Out     | Total            |     |
| General Light Industrial | 110         | 112,525   | 73                | 10  | 83    | 10    | 63      | 73               | 548 |

Given that the surrounding site vicinity is primarily industrial in character, the nearby transportation system was constructed to serve the needs of existing and future industrial development. As such, it is expected that a majority of trips would utilize the transportation corridors of SW Tualatin-Sherwood Road and SW Teton Avenue. From SW Tualatin-Sherwood Road and SW Teton Avenue, access to regional transportation facilities, such as SW Pacific Highway, SW Boones Ferry Road (OR-141), Interstate 5, and Interstate 205, are available.

### Trip Distribution

The following trip distribution was estimated based on existing traffic volumes, the locations of likely trip destinations, and locations of major transportation facilities in the site vicinity:

- Approximately 45 percent of site trips will travel to/from the east along SW Tualatin-Sherwood Road;
- Approximately 35 percent of site trips will travel to/from the west along SW Tualatin-Sherwood Road;
- Approximately 10 percent of site trips will travel to/from the north along SW Teton Avenue; and
- Approximately 10 percent of site trips will travel to/from the south along SW Teton Avenue.

Staff provided a general guideline of 60 peak hour trips and 500 daily trips through an intersection during the scoping phase for a previous project (*Tualatin Logistics Traffic Study Scoping Memorandum – Revised*, June 18,



<sup>&</sup>lt;sup>1</sup> Institute of Transportation Engineers (ITE), *Trip Generation Manual*, 11<sup>th</sup> Edition, 2021.

2021). Washington County (Resolution & Order 86-95) defines the impact area for developments as "those road links where site-generated traffic equals or exceeds 10% of existing average daily traffic" (ADT).

Table 4 summarizes the estimated number of additional trips through nearby intersections based on the trip distribution described above. No intersections are expected to have more additional trips than the 60 peak hour trip threshold or be over the 500 daily trip threshold.

| Intersection  | Site Trip    | Net Site Trips |       |  |
|---|--------------|----------------|-------|--|
| Intersection  | Distribution | Peak Hour      | Daily |  |
| SW 124 <sup>th</sup> Avenue & SW Tualatin-Sherwood Road                 | 35%          | 29             | 192   |  |
| SW 112 <sup>th</sup> Avenue/SW Avery Street & SW Tualatin-Sherwood Road | 35%          | 29             | 192   |  |
| SW Teton Avenue & SW Tualatin-Sherwood Road                             | 65%          | 54             | 356   |  |
| SW Boones Ferry Road at SW Tualatin-Sherwood Road                       | 45%          | 37             | 247   |  |

#### Table 4: Additional Peak Hour and Weekday Trips Summary

Traffic data from the Oregon Department of Transportation's (ODOT) TransGIS website was reviewed to determine where daily site trips are anticipated to exceed ten percent of the existing ADT and identify intersections to be analyzed in the TIA. Table 5 summarizes the ADT on roadways within the site vicinity and the estimated site trips on the subject roadways.

#### Table 5: Weekday Site Trips and Existing ADT Summary

| Roadway                       | Point   | Site Trip<br>Distribution | Site Trips | Existing<br>ADT | Ratio of Site Trips to<br>Existing ADT (%) |
|-------------------------------|---|---------------------------|------------|-----------------|--|
| SW Tualatin-<br>Sherwood Road | East of SW 124 <sup>th</sup> Avenue,<br>west of SW 120 <sup>th</sup> Avenue | 35%                       | 192        | 29,900          | 0.6%                                       |
| SW Tualatin-<br>Sherwood Road | 0.01 mile west of<br>SW Boones Ferry Road                                   | 45%                       | 247        | 34,300          | 0.7%                                       |

Note: Existing ADT based on ODOT TransGIS Traffic Data

Considering the net increase in traffic on area roadways, none of the nearby intersections or roadways are anticipated to sustain a significant increase in traffic volume or meet the volume threshold guidelines provided by Staff. Therefore, no off-site intersections are proposed for analysis as part of this report.

The trip distribution and assignment for the total site trips generated during the morning and evening peak hours is shown in Figure 3.



#### LEGEND

 XX%
 PERCENT OF PROJECT TRIPS

 TRIP GENERATION
 IN

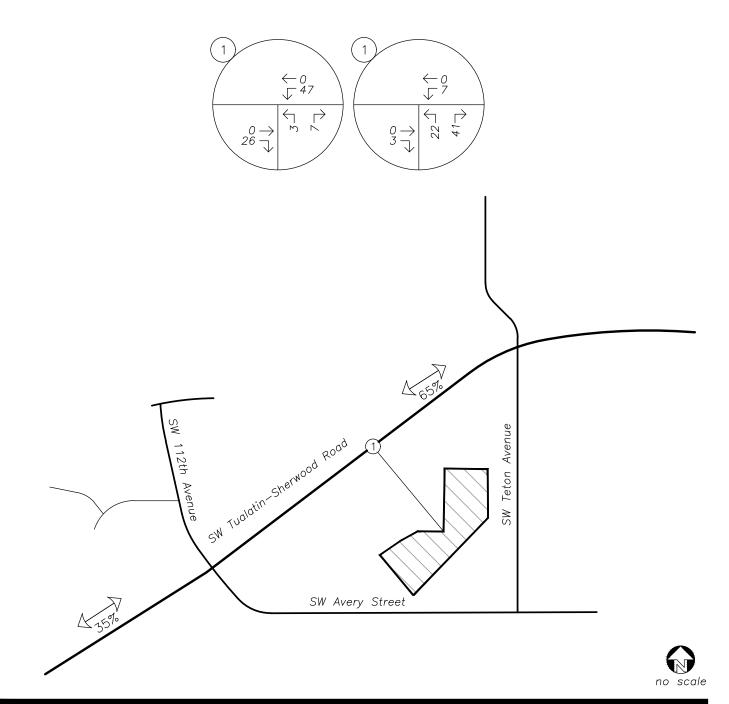
 IN
 OUT
 TOTAL

 AM
 73
 10
 83

 PM
 10
 63
 73

AM PEAK HOUR

PM PEAK HOUR





#### SITE TRIP DISTRIBUTION & ASSIGNMENT

Proposed Development Plan - Site Trips AM & PM Peak Hours Figure 3 Avery | & || 2/8/2022

### **Traffic Volumes**

### Existing Conditions

Traffic counts were conducted at the study intersection on Thursday, February 10, 2022, from 7:00 AM to 9:00 AM and from 4:00 PM to 6:00 PM. Data was used from the intersection's respective morning and evening peak hours. Raw count data is included in Appendix B.

The ongoing COVID-19 viral pandemic, which began in March 2020, has initiated a significant decrease in traffic due to policies on social distancing that have closed or limited business operations and reduced commuting as many people work from home. A comparison of the Portland State University (PSU) Portal data for the I-5 interchange on-ramps near the project site shows that most volumes are at most about 1 percent lower at the end of October 2021 as compared with the same period in 2019. As a result, new traffic data collected for this project was not adjusted for "normal" conditions, as current traffic volumes are close to pre-COVID volumes.

Figure 4 shows the existing traffic volumes at the study intersection for the morning and evening peak hours.

### Background Conditions

To provide analysis of the impact of the proposed development on the nearby transportation facilities, an estimate of future traffic volumes is required. A compounded growth rate of two percent per year for an assumed buildout condition of one year was applied to the measured existing traffic volumes to approximate general growth for year 2023 background conditions.

In addition to the traffic volume growth described above, trips associated with two in-process developments within the site vicinity<sup>2</sup>, that are currently approved but not yet fully constructed or occupied, were added to the existing volumes in addition to the calculated volume growth. The following projects were assumed to be completed and occupied prior to year 2023:

- PGE Integrated Operations Center;
- Sherwood Industrial Park;
- Manhasset Industrial (10500 SW Manhasset Drive); and
- Tualatin Industrial Park (11045 SW Tualatin-Sherwood Road)

Figures depicting trip assignment associated with the in-process developments are included in Appendix B.

Figure 5 shows the projected year 2023 background volumes at the study intersection for the morning and evening peak hours.



<sup>&</sup>lt;sup>2</sup> https://www.tualatinoregon.gov/projects

### Buildout Conditions

The trips estimated to be generated by the proposed development, as described earlier within the *Site Trips* section, were added to the year 2023 background traffic volumes to estimate traffic volumes under the year 2023 buildout conditions.

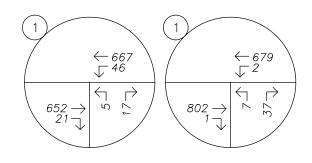
Figure 6 shows the projected year 2023 buildout volumes at the study intersection for the morning and evening peak hours.

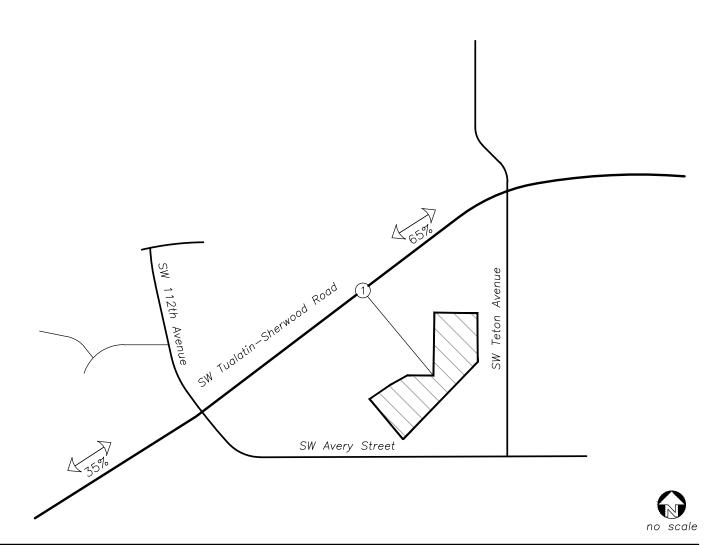
### Future Roadway Improvements

Improvements along Tualatin-Sherwood Road (between Teton Avenue and Langer Farms Parkway) are planned to begin in 2022 and finish by 2025. As part of this project, the roadway will be widened to five travel lanes (two travel lanes in each direction and a center-turn lane) and bicycle and pedestrian facilities will be included along both sides of the roadway.



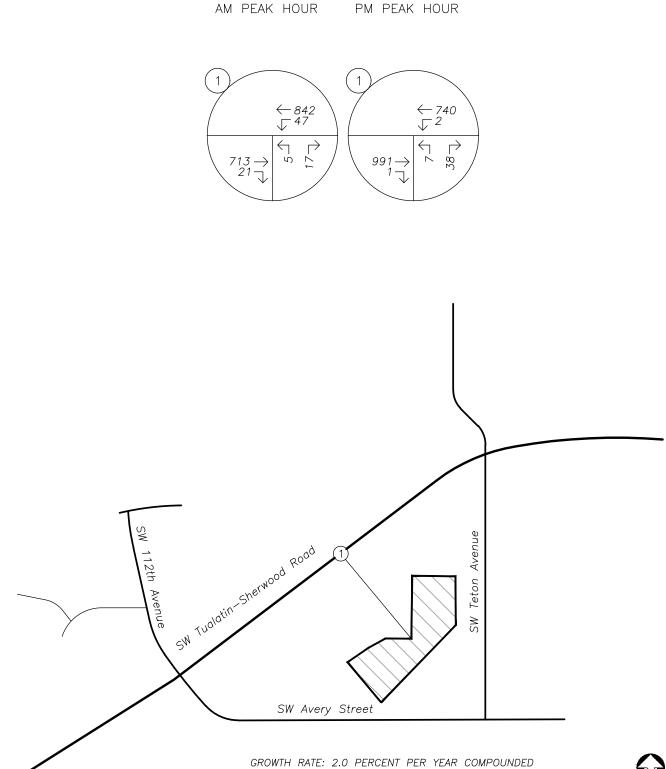
#### AM PEAK HOUR







**TRAFFIC VOLUMES** Year 2022 Existing Conditions AM & PM Peak Hours Figure 4 Avery I & II 2/15/2022



no scale

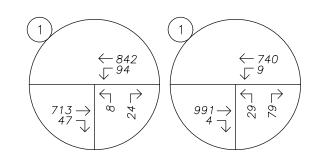


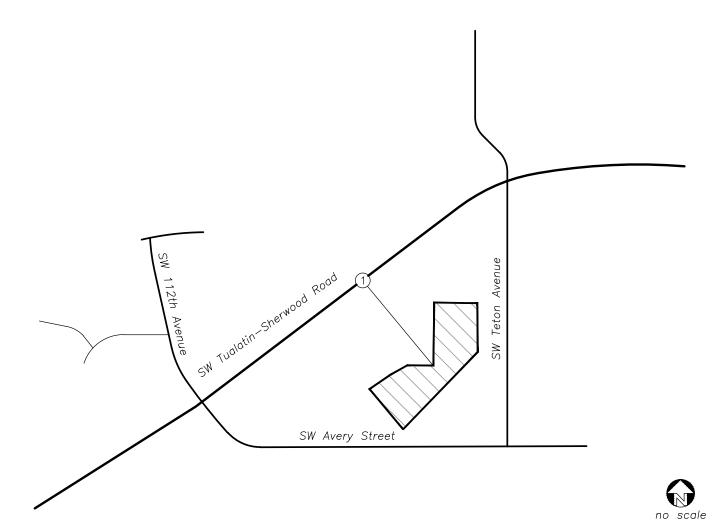
TRAFFIC VOLUMES

Year 2023 Background Conditions AM & PM Peak Hours Figure 5 Avery | & || 2/15/2022

#### AM PEAK HOUR







lancaster mobley **TRAFFIC VOLUMES** Year 2023 Buildout Conditions AM & PM Peak Hours Figure 6 Avery | & || 2/15/2022

### Safety Analysis

### Crash History Review

Using data obtained from the ODOT's Crash Data System, the most recent available five years of crash history (January 2015 to December 2019) at the study intersection was reviewed. The crash data were evaluated based on the number of crashes, the type of collisions, the severity of the collisions, and the resulting crash rate for the intersection.

Crash severity is based on injuries sustained by people involved in the crash. ODOT classifies crash severity into the following five categories:

- Property Damage Only (PDO)
- Possible Injury (Injury C)
- Non-Incapacitating Injury (*Injury B*)
- Incapacitating Injury (*Injury A*)
- Fatality or Fatal Injury

Crash rates provide the ability to compare safety risks at different intersections by accounting for both the number of crashes that have occurred during the study period and the number of vehicles that typically travel through the intersection. Crash rates were calculated using the common assumption that traffic counted during the evening peak period represents approximately 10 percent of the annual average daily traffic (AADT) at the intersection.

Table 6 provides a summary of collision types, crash severities, and the calculated crash rate for the study intersection. Detailed ODOT crash reports are included in Appendix C.

|   | Internetion                                     | Collisic | on Type |     | Cras | sh Seve | rity |       | Total   | AADT   | Crash<br>Rate |
|---|---|----------|---------|-----|------|---------|------|-------|---------|--------|---------------|
|   | Intersection                                    | Turn     | Other   | PDO | С    | В       | Α    | Fatal | Crashes |        |               |
| 1 | Site Access at<br>SW Tualatin-<br>Sherwood Road | 1        | 0       | 1   | 0    | 0       | 0    | 0     | 1       | 15,280 | 0.036         |

#### Table 6: Crash Type Summary

Based on a review of the available crash data and crash rates, patterns are consistent with the geometry and traffic control provided at the study intersection. The proposed project is not expected to change or worsen crash rates. Accordingly, no safety mitigation is recommended per the crash data analysis.

### Warrant Analysis

Left-turn lane warrants and preliminary traffic signal warrants were examined for the study intersection where such treatments would be applicable.



#### Left-Turn Lane Warrants

Left-turn lane warrants were not examined for the westbound approach from SW Tualatin-Sherwood Road into the site as the roadway has an existing two-way left-turn lane as part of the roadway cross-section.

#### Preliminary Traffic Signal Warrants

Preliminary traffic signal warrants were examined at the site access intersection to determine whether the installation of a new traffic signal will be warranted at this intersection upon completion of the proposed development.

Traffic signal warrants are not met this intersection under buildout conditions. Detailed information on the warrant analysis is included in Appendix C.

### Sight Distance

Sight distance was not measured and evaluated, as the proposed development will be using an existing access

### **Operational Analysis**

A capacity and delay analysis was conducted for the study intersection per the unsignalized intersection analysis methodologies in the *Highway Capacity Manual* (HCM) 6<sup>th</sup> Edition<sup>3</sup>. Intersections are generally evaluated based on the average control delay experienced by vehicles and are assigned a grade according to their operation. The level of service (LOS) of an intersection can range from LOS A, which indicates very little or no delay experienced by vehicles a high degree of congestion and delay. The volume-to-capacity (v/c) ratio is a measure that compares the traffic volumes (demand) against the available capacity of an intersection.

### Performance Standards

Intersections along SW Tualatin-Sherwood Road are under the jurisdiction of Washington County, where the County requires intersections to operate with a v/c ratio of 0.99 or less.

### Delay & Capacity Analysis

The LOS, delay, and v/c results of the capacity analysis are shown in Table 7. Detailed calculations as well as tables showing the relationship between delay and LOS are included in Appendix D.



<sup>&</sup>lt;sup>3</sup> Transportation Research Board, *Highway Capacity Manual*, 6<sup>th</sup> Edition, 2016.

#### Table 7: Intersection Capacity Analysis Summary

| Condition                 | Мс   | orning Peak H | our  | Evening Peak Hour |           |      |  |  |  |  |  |
|---------------------------|--|---------------|------|-------------------|-----------|------|--|--|--|--|--|
| Condition                 | LOS  | Delay (s)     | v/c  | LOS               | Delay (s) | v/c  |  |  |  |  |  |
| 1. Si                     | 1. Site Access (Existing) at SW Tualatin-Sherwood Road |               |      |                   |           |      |  |  |  |  |  |
| 2021 Existing Condition   | С  | 16            | 0.07 | С                 | 17        | 0.13 |  |  |  |  |  |
| 2023 Background Condition | С  | 17            | 0.08 | С                 | 21        | 0.18 |  |  |  |  |  |
| 2023 Buildout Condition   | С  | 19            | 0.13 | D                 | 30        | 0.44 |  |  |  |  |  |

The study intersection is currently operating acceptably per Washington County standards and is projected to continue operating acceptably through the 2023 buildout year of the site. No operational mitigation is required or recommended.

This project will be completed prior to the construction of the planned five lane cross-section on SW Tualatin-Sherwood Road. However, a review of operations with the future configuration shows that operations are not adversely impacted at the site driveway when the widening of SW Tualatin-Sherwood Road is completed.

### Conclusions

Key findings of this study include:

- The proposed development is estimated to generate 83 morning peak hour, 73 evening peak hour, and 548 average weekday trips.
- Based on a review of the available crash data and crash rates, patterns are consistent with the geometry and traffic control provided at the study intersection. The proposed project is not expected to change or worsen crash rates. Accordingly, no safety mitigation is recommended per the crash data analysis.
- Preliminary traffic signal warrants are not met at the unsignalized study area intersection under buildout conditions.
- The study intersection is currently operating acceptably per Washington County standards and is projected to continue operating acceptably through the 2023 buildout year of the site. No operational mitigation is required or recommended.
- The construction of the planned five lane cross-section on SW Tualatin-Sherwood Road will not adversely affect future operations at the study intersection.



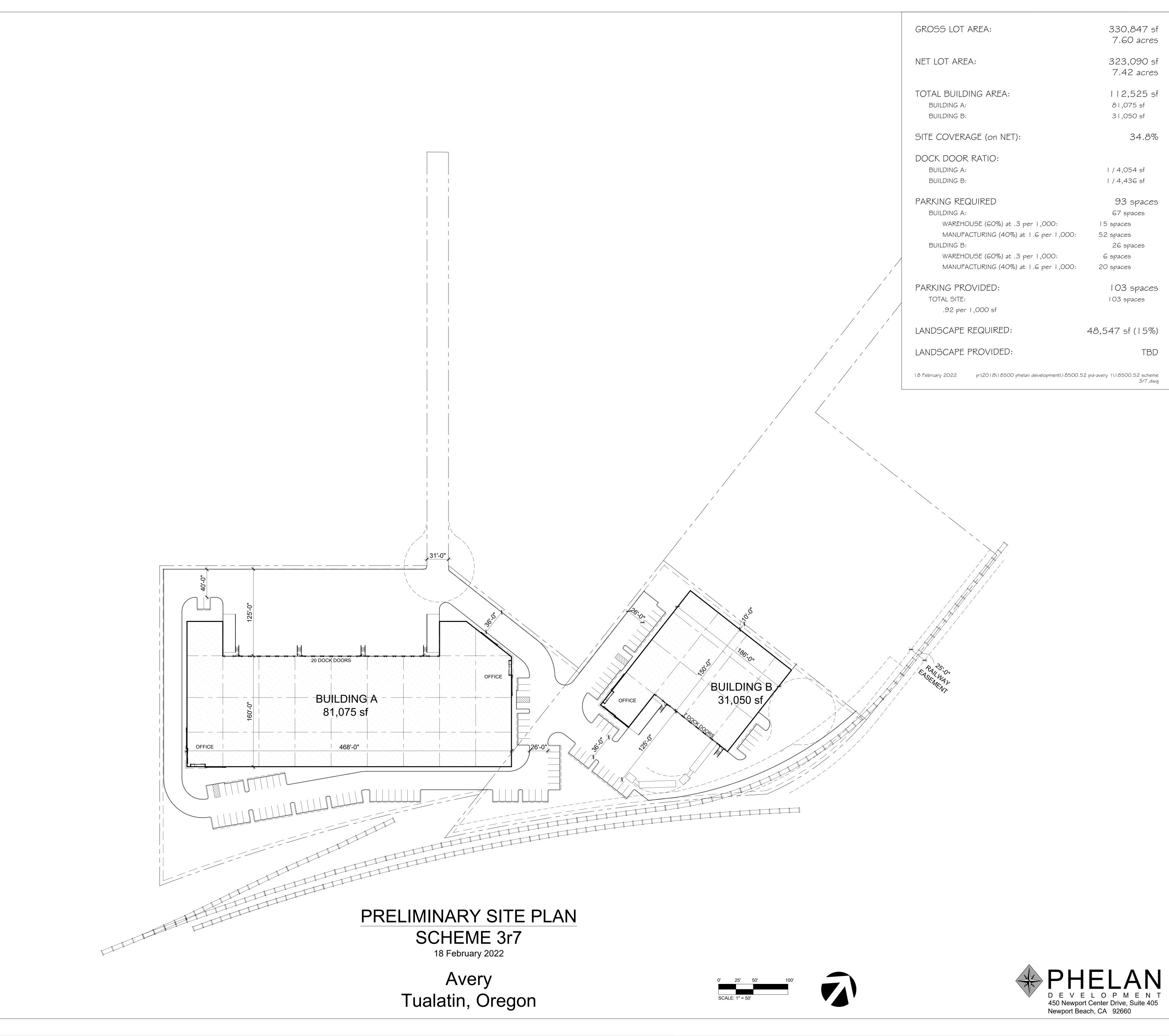
# Appendix A – Site Information

Site Plan

Trip Generation Calculations







330,847 sf 7.60 acres 112,525 sf 103 spaces



#### TRIP GENERATION CALCULATIONS Source: Trip Generation Manual, 11th Edition

Land Use:General Light IndustrialLand Use Code:110Land Use Subcategory:All SitesSetting/LocationGeneral Urban/SuburbanVariable:1000 SF GFATrip Type:VehicleVariable Quantity:112.6

#### AM PEAK HOUR

Trip Rate: 0.74

|                   | Enter | Exit | Total |
|-------------------|-------|------|-------|
| Directional Split | 88%   | 12%  |       |
| Trip Ends         | 73    | 10   | 83    |

#### WEEKDAY

Trip Rate: 4.87

|                   | Enter | Exit | Total |
|-------------------|-------|------|-------|
| Directional Split | 50%   | 50%  |       |
| Trip Ends         | 274   | 274  | 548   |

# PM PEAK HOUR

Trip Rate: 0.65

|                   | Enter | Exit | Total |
|-------------------|-------|------|-------|
| Directional Split | 14%   | 86%  |       |
| Trip Ends         | 10    | 63   | 73    |

#### SATURDAY

Trip Rate: 0.69

|                   | Enter | Exit | Total |
|-------------------|-------|------|-------|
| Directional Split | 50%   | 50%  |       |
| Trip Ends         | 39    | 39   | 78    |

# Appendix B – Traffic Data

Turning Movement Counts

In-Process Traffic Data





Location: 1 Stie Access & SW Tualatin Sherwood Rd AM

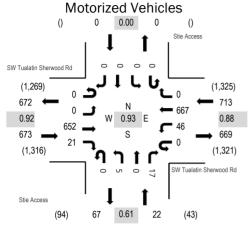
Date: Thursday, February 10, 2022

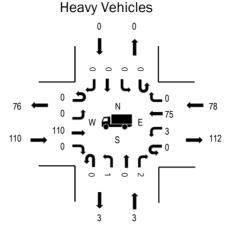
Study Peak Hour: 07:25 AM - 08:25 AM

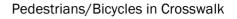
Peak 15-Minutes in Study Peak Hour:

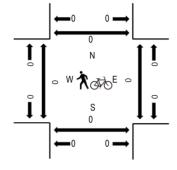
07:40 AM - 07:55 AM

#### Study Peak Hour (for all study intersections)









Note: Total study counts contained in parentheses.

|     | ,     |      |
|-----|-------|------|
|     | HV%   | PHF  |
| EB  | 16.3% | 0.92 |
| WB  | 10.9% | 0.88 |
| NB  | 13.6% | 0.61 |
| SB  | 0.0%  | 0.00 |
| All | 13.6% | 0.93 |
|     |       |      |

#### **Traffic Counts - Motorized Vehicles**

| Interval    |        | East | n Sherwoo<br>bound |       |        | West | Sherwoo<br>bound |       |        | North | occess<br>bound |       |        | South | ccess |       | _     | Rolling |
|-------------|--------|------|--------------------|-------|--------|------|------------------|-------|--------|-------|-----------------|-------|--------|-------|-------|-------|-------|---------|
| Start Time  | U-Turn | Left | Thru               | Right | U-Turn | Left | Thru             | Right | U-Turn | Left  | Thru            | Right | U-Turn | Left  | Thru  | Right | Total | Hour    |
| 7:00 AM     | 0      | 0    | 47                 | 1     | 0      | 0    | 54               | 0     | 0      | 0     | 0               | 0     | 0      | 0     | 0     | 0     | 102   | 1,368   |
| 7:05 AM     | 0      | 0    | 54                 | 0     | 0      | 2    | 50               | 0     | 0      | 0     | 0               | 3     | 0      | 0     | 0     | 0     | 109   | 1,384   |
| 7:10 AM     | 0      | 0    | 56                 | 0     | 0      | 2    | 55               | 0     | 0      | 0     | 0               | 2     | 0      | 0     | 0     | 0     | 115   | 1,364   |
| 7:15 AM     | 0      | 0    | 62                 | 0     | 0      | 1    | 39               | 0     | 0      | 0     | 0               | 0     | 0      | 0     | 0     | 0     | 102   | 1,380   |
| 7:20 AM     | 0      | 0    | 44                 | 0     | 0      | 2    | 46               | 0     | 0      | 0     | 0               | 3     | 0      | 0     | 0     | 0     | 95    | 1,391   |
| 7:25 AM     | 0      | 0    | 50                 | 2     | 0      | 3    | 69               | 0     | 0      | 0     | 0               | 0     | 0      | 0     | 0     | 0     | 124   | 1,408   |
| 7:30 AM     | 0      | 0    | 54                 | 1     | 0      | 4    | 62               | 0     | 0      | 0     | 0               | 3     | 0      | 0     | 0     | 0     | 124   | 1,402   |
| 7:35 AM     | 0      | 0    | 56                 | 4     | 0      | 5    | 60               | 0     | 0      | 0     | 0               | 1     | 0      | 0     | 0     | 0     | 126   | 1,389   |
| 7:40 AM     | 0      | 0    | 62                 | 1     | 0      | 0    | 37               | 0     | 0      | 0     | 0               | 0     | 0      | 0     | 0     | 0     | 100   | 1,371   |
| 7:45 AM     | 0      | 0    | 55                 | 1     | 0      | 5    | 79               | 0     | 0      | 0     | 0               | 1     | 0      | 0     | 0     | 0     | 141   | 1,365   |
| 7:50 AM     | 0      | 0    | 53                 | 2     | 0      | 7    | 71               | 0     | 0      | 1     | 0               | 2     | 0      | 0     | 0     | 0     | 136   | 1,318   |
| 7:55 AM     | 0      | 0    | 52                 | 4     | 0      | 5    | 32               | 0     | 0      | 0     | 0               | 1     | 0      | 0     | 0     | 0     | 94    | 1,288   |
| 8:00 AM     | 0      | 0    | 45                 | 1     | 0      | 4    | 65               | 0     | 0      | 0     | 0               | 3     | 0      | 0     | 0     | 0     | 118   | 1,316   |
| 8:05 AM     | 0      | 0    | 46                 | 1     | 0      | 2    | 39               | 0     | 0      | 1     | 0               | 0     | 0      | 0     | 0     | 0     | 89    |         |
| 8:10 AM     | 0      | 0    | 58                 | 1     | 0      | 7    | 62               | 0     | 0      | 1     | 0               | 2     | 0      | 0     | 0     | 0     | 131   |         |
| 8:15 AM     | 0      | 0    | 54                 | 1     | 0      | 1    | 55               | 0     | 0      | 1     | 0               | 1     | 0      | 0     | 0     | 0     | 113   |         |
| 8:20 AM     | 0      | 0    | 67                 | 2     | 0      | 3    | 36               | 0     | 0      | 1     | 0               | 3     | 0      | 0     | 0     | 0     | 112   |         |
| 8:25 AM     | 0      | 0    | 58                 | 2     | 0      | 2    | 53               | 0     | 0      | 1     | 0               | 2     | 0      | 0     | 0     | 0     | 118   |         |
| 8:30 AM     | 0      | 0    | 62                 | 0     | 0      | 1    | 48               | 0     | 0      | 0     | 0               | 0     | 0      | 0     | 0     | 0     | 111   |         |
| 8:35 AM     | 0      | 0    | 47                 | 0     | 0      | 3    | 57               | 0     | 0      | 1     | 0               | 0     | 0      | 0     | 0     | 0     | 108   |         |
| 8:40 AM     | 0      | 0    | 53                 | 0     | 0      | 0    | 38               | 0     | 0      | 0     | 0               | 3     | 0      | 0     | 0     | 0     | 94    |         |
| 8:45 AM     | 0      | 0    | 43                 | 0     | 0      | 1    | 50               | 0     | 0      | 0     | 0               | 0     | 0      | 0     | 0     | 0     | 94    |         |
| 8:50 AM     | 0      | 0    | 56                 | 3     | 0      | 5    | 38               | 0     | 0      | 2     | 0               | 2     | 0      | 0     | 0     | 0     | 106   |         |
| 8:55 AM     | 0      | 0    | 54                 | 1     | 0      | 1    | 64               | 0     | 0      | 1     | 0               | 1     | 0      | 0     | 0     | 0     | 122   |         |
| Count Total | 0      | 0    | 1,288              | 28    | 0      | 66   | 1,259            | 0     | 0      | 10    | 0               | 33    | 0      | 0     | 0     | 0     | 2,684 |         |
| Peak Hour   | 0      | 0    | 652                | 21    | 0      | 46   | 667              | 0     | 0      | 5     | 0               | 17    | 0      | 0     | 0     | 0     | 1,408 | }       |

#### Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles on Crosswalk

| Interval    |     | Hea | avy Vehicle | es |       | Interval    |    | Bicycle | es on Road | lway |       | Interval    | Peo | destrians/E | Bicycles on | Crosswa | lk    |
|-------------|-----|-----|-------------|----|-------|-------------|----|---------|------------|------|-------|-------------|-----|-------------|-------------|---------|-------|
| Start Time  | EB  | NB  | WB          | SB | Total | Start Time  | EB | NB      | WB         | SB   | Total | Start Time  | EB  | NB          | WB          | SB      | Total |
| 7:00 AM     | 12  | 0   | 7           | 0  | 19    | 7:00 AM     | 0  | 0       | 0          | 0    | 0     | 7:00 AM     | 0   | 0           | 0           | 0       | 0     |
| 7:05 AM     | 9   | 0   | 3           | 0  | 12    | 7:05 AM     | 0  | 0       | 0          | 0    | 0     | 7:05 AM     | 0   | 0           | 0           | 0       | 0     |
| 7:10 AM     | 9   | 1   | 6           | 0  | 16    | 7:10 AM     | 0  | 0       | 0          | 0    | 0     | 7:10 AM     | 0   | 0           | 0           | 0       | 0     |
| 7:15 AM     | 12  | 0   | 8           | 0  | 20    | 7:15 AM     | 0  | 0       | 0          | 0    | 0     | 7:15 AM     | 0   | 0           | 0           | 0       | 0     |
| 7:20 AM     | 7   | 0   | 4           | 0  | 11    | 7:20 AM     | 0  | 0       | 2          | 0    | 2     | 7:20 AM     | 0   | 0           | 0           | 0       | 0     |
| 7:25 AM     | 17  | 0   | 7           | 0  | 24    | 7:25 AM     | 0  | 0       | 0          | 0    | 0     | 7:25 AM     | 0   | 0           | 0           | 0       | 0     |
| 7:30 AM     | 9   | 1   | 3           | 0  | 13    | 7:30 AM     | 0  | 0       | 0          | 0    | 0     | 7:30 AM     | 0   | 0           | 0           | 0       | 0     |
| 7:35 AM     | 11  | 1   | 5           | 0  | 17    | 7:35 AM     | 0  | 0       | 1          | 0    | 1     | 7:35 AM     | 0   | 0           | 0           | 0       | 0     |
| 7:40 AM     | 9   | 0   | 5           | 0  | 14    | 7:40 AM     | 0  | 0       | 0          | 0    | 0     | 7:40 AM     | 0   | 0           | 0           | 0       | 0     |
| 7:45 AM     | 9   | 0   | 9           | 0  | 18    | 7:45 AM     | 0  | 0       | 0          | 0    | 0     | 7:45 AM     | 0   | 0           | 0           | 0       | 0     |
| 7:50 AM     | 7   | 0   | 8           | 0  | 15    | 7:50 AM     | 0  | 0       | 0          | 0    | 0     | 7:50 AM     | 0   | 0           | 0           | 0       | 0     |
| 7:55 AM     | 5   | 0   | 4           | 0  | 9     | 7:55 AM     | 0  | 0       | 0          | 0    | 0     | 7:55 AM     | 0   | 0           | 0           | 0       | 0     |
| 8:00 AM     | 8   | 0   | 9           | 0  | 17    | 8:00 AM     | 0  | 0       | 0          | 0    | 0     | 8:00 AM     | 0   | 0           | 0           | 0       | 0     |
| 8:05 AM     | 5   | 0   | 4           | 0  | 9     | 8:05 AM     | 0  | 0       | 0          | 0    | 0     | 8:05 AM     | 0   | 0           | 0           | 0       | 0     |
| 8:10 AM     | 10  | 0   | 10          | 0  | 20    | 8:10 AM     | 0  | 0       | 0          | 0    | 0     | 8:10 AM     | 0   | 0           | 0           | 0       | 0     |
| 8:15 AM     | 10  | 0   | 6           | 0  | 16    | 8:15 AM     | 0  | 0       | 0          | 0    | 0     | 8:15 AM     | 0   | 0           | 0           | 0       | 0     |
| 8:20 AM     | 10  | 1   | 8           | 0  | 19    | 8:20 AM     | 1  | 0       | 0          | 0    | 1     | 8:20 AM     | 0   | 0           | 0           | 0       | 0     |
| 8:25 AM     | 7   | 1   | 4           | 0  | 12    | 8:25 AM     | 0  | 0       | 0          | 0    | 0     | 8:25 AM     | 0   | 0           | 0           | 0       | 0     |
| 8:30 AM     | 8   | 0   | 9           | 0  | 17    | 8:30 AM     | 0  | 0       | 0          | 0    | 0     | 8:30 AM     | 0   | 0           | 0           | 0       | 0     |
| 8:35 AM     | 4   | 0   | 10          | 0  | 14    | 8:35 AM     | 0  | 0       | 0          | 0    | 0     | 8:35 AM     | 0   | 0           | 0           | 0       | 0     |
| 8:40 AM     | 7   | 0   | 5           | 0  | 12    | 8:40 AM     | 0  | 0       | 0          | 0    | 0     | 8:40 AM     | 0   | 0           | 0           | 0       | 0     |
| 8:45 AM     | 10  | 0   | 8           | 0  | 18    | 8:45 AM     | 0  | 0       | 0          | 0    | 0     | 8:45 AM     | 0   | 0           | 0           | 0       | 0     |
| 8:50 AM     | 10  | 0   | 5           | 0  | 15    | 8:50 AM     | 0  | 0       | 0          | 0    | 0     | 8:50 AM     | 0   | 0           | 0           | 0       | 0     |
| 8:55 AM     | 8   | 0   | 5           | 0  | 13    | 8:55 AM     | 0  | 0       | 0          | 0    | 0     | 8:55 AM     | 0   | 0           | 0           | 0       | 0     |
| Count Total | 213 | 5   | 152         | 0  | 370   | Count Total | 1  | 0       | 3          | 0    | 4     | Count Total | 0   | 0           | 0           | 0       | 0     |
| Peak Hour   | 110 | 3   | 78          | 0  | 191   | Peak Hour   | 1  | 0       | 1          | 0    | 2     | Peak Hour   | 0   | 0           | 0           | 0       | 0     |



Location: 1 Stie Access & SW Tualatin Sherwood Rd PM

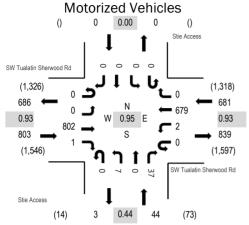
Date: Thursday, February 10, 2022

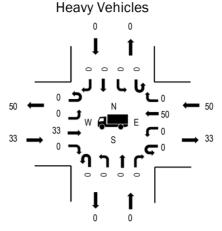
Study Peak Hour: 04:45 PM - 05:45 PM

Peak 15-Minutes in Study Peak Hour:

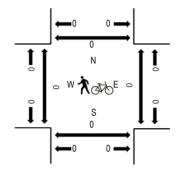
05:30 PM - 05:45 PM

#### Study Peak Hour (for all study intersections)





#### Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.

|     |      |      | J |
|-----|------|------|---|
|     | HV%  | PHF  |   |
| EB  | 4.1% | 0.93 |   |
| WB  | 7.3% | 0.93 |   |
| NB  | 0.0% | 0.44 |   |
| SB  | 0.0% | 0.00 |   |
| All | 5.4% | 0.95 |   |
|     |      |      |   |

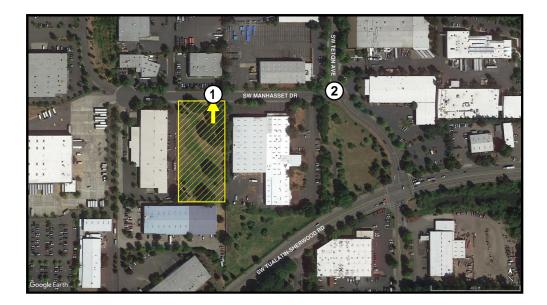
#### **Traffic Counts - Motorized Vehicles**

|             |        | 11200 | 101110  |       |        |      |         |       |        |        |       |       |        |        |       |       |       |         |
|-------------|--------|-------|---------|-------|--------|------|---------|-------|--------|--------|-------|-------|--------|--------|-------|-------|-------|---------|
|             | SW     |       | Sherwoo | od Rd | SW     |      | Sherwoo | od Rd |        | Stie A |       |       |        | Stie A |       |       |       |         |
| Interval    |        |       | bound   |       |        |      | bound   |       |        |        | bound |       |        |        | bound |       |       | Rolling |
| Start Time  | U-Turn | Left  | Thru    | Right | U-Turn | Left | Thru    | Right | U-Turn | Left   | Thru  | Right | U-Turn | Left   | Thru  | Right | Total | Hour    |
| 4:00 PM     | 0      | 0     | 74      | 0     | 0      | 0    | 44      | 0     | 0      | 0      | 0     | 4     | 0      | 0      | 0     | 0     | 122   | 1,455   |
| 4:05 PM     | 0      | 0     | 64      | 0     | 0      | 0    | 56      | 0     | 0      | 0      | 0     | 3     | 0      | 0      | 0     | 0     | 123   | 1,476   |
| 4:10 PM     | 0      | 0     | 69      | 1     | 0      | 0    | 69      | 0     | 0      | 1      | 0     | 2     | 0      | 0      | 0     | 0     | 142   | 1,470   |
| 4:15 PM     | 0      | 0     | 47      | 1     | 0      | 0    | 59      | 0     | 0      | 0      | 0     | 1     | 0      | 0      | 0     | 0     | 108   | 1,452   |
| 4:20 PM     | 0      | 0     | 61      | 0     | 0      | 1    | 52      | 0     | 0      | 0      | 0     | 1     | 0      | 0      | 0     | 0     | 115   | 1,484   |
| 4:25 PM     | 0      | 0     | 69      | 0     | 0      | 5    | 55      | 0     | 0      | 1      | 0     | 3     | 0      | 0      | 0     | 0     | 133   | 1,504   |
| 4:30 PM     | 0      | 0     | 63      | 0     | 0      | 0    | 67      | 0     | 0      | 3      | 0     | 1     | 0      | 0      | 0     | 0     | 134   | 1,483   |
| 4:35 PM     | 0      | 0     | 56      | 1     | 0      | 1    | 38      | 0     | 0      | 2      | 0     | 0     | 0      | 0      | 0     | 0     | 98    | 1,479   |
| 4:40 PM     | 0      | 0     | 64      | 0     | 0      | 0    | 54      | 0     | 0      | 2      | 0     | 4     | 0      | 0      | 0     | 0     | 124   | 1,507   |
| 4:45 PM     | 0      | 0     | 58      | 0     | 0      | 0    | 66      | 0     | 0      | 0      | 0     | 1     | 0      | 0      | 0     | 0     | 125   | 1,528   |
| 4:50 PM     | 0      | 0     | 64      | 0     | 0      | 1    | 50      | 0     | 0      | 2      | 0     | 5     | 0      | 0      | 0     | 0     | 122   | 1,515   |
| 4:55 PM     | 0      | 0     | 58      | 0     | 0      | 0    | 45      | 0     | 0      | 2      | 0     | 4     | 0      | 0      | 0     | 0     | 109   | 1,497   |
| 5:00 PM     | 0      | 0     | 78      | 0     | 0      | 0    | 53      | 0     | 0      | 1      | 0     | 11    | 0      | 0      | 0     | 0     | 143   | 1,482   |
| 5:05 PM     | 0      | 0     | 54      | 0     | 0      | 0    | 59      | 0     | 0      | 0      | 0     | 4     | 0      | 0      | 0     | 0     | 117   |         |
| 5:10 PM     | 0      | 0     | 73      | 0     | 0      | 0    | 44      | 0     | 0      | 2      | 0     | 5     | 0      | 0      | 0     | 0     | 124   |         |
| 5:15 PM     | 0      | 0     | 59      | 0     | 0      | 0    | 78      | 0     | 0      | 0      | 0     | 3     | 0      | 0      | 0     | 0     | 140   |         |
| 5:20 PM     | 0      | 0     | 78      | 0     | 0      | 0    | 56      | 0     | 0      | 0      | 0     | 1     | 0      | 0      | 0     | 0     | 135   |         |
| 5:25 PM     | 0      | 0     | 66      | 0     | 0      | 1    | 45      | 0     | 0      | 0      | 0     | 0     | 0      | 0      | 0     | 0     | 112   |         |
| 5:30 PM     | 0      | 0     | 58      | 1     | 0      | 0    | 70      | 0     | 0      | 0      | 0     | 1     | 0      | 0      | 0     | 0     | 130   |         |
| 5:35 PM     | 0      | 0     | 74      | 0     | 0      | 0    | 50      | 0     | 0      | 0      | 0     | 2     | 0      | 0      | 0     | 0     | 126   |         |
| 5:40 PM     | 0      | 0     | 82      | 0     | 0      | 0    | 63      | 0     | 0      | 0      | 0     | 0     | 0      | 0      | 0     | 0     | 145   |         |
| 5:45 PM     | 0      | 0     | 67      | 0     | 0      | 0    | 45      | 0     | 0      | 0      | 0     | 0     | 0      | 0      | 0     | 0     | 112   |         |
| 5:50 PM     | 0      | 0     | 59      | 0     | 0      | 0    | 45      | 0     | 0      | 0      | 0     | 0     | 0      | 0      | 0     | 0     | 104   |         |
| 5:55 PM     | 0      | 0     | 46      | 1     | 0      | 0    | 46      | 0     | 0      | 1      | 0     | 0     | 0      | 0      | 0     | 0     | 94    |         |
| Count Total | 0      | 0     | 1,541   | 5     | 0      | 9    | 1,309   | 0     | 0      | 17     | 0     | 56    | 0      | 0      | 0     | 0     | 2,937 | _       |
| Peak Hour   | 0      | 0     | 802     | 1     | 0      | 2    | 679     | 0     | 0      | 7      | 0     | 37    | 0      | 0      | 0     | 0     | 1,528 |         |

#### Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles on Crosswalk

| Interval    |    | Неа | avy Vehicle | es | •     | Interval    |    | Bicycle | es on Road | lway |       | Interval    | Peo | destrians/E | Bicycles on | Crosswa | lk    |
|-------------|----|-----|-------------|----|-------|-------------|----|---------|------------|------|-------|-------------|-----|-------------|-------------|---------|-------|
| Start Time  | EB | NB  | WB          | SB | Total | Start Time  | EB | NB      | WB         | ŚB   | Total | Start Time  | EB  | NB          | WB          | SB      | Total |
| 4:00 PM     | 4  | 0   | 3           | 0  | 7     | 4:00 PM     | 0  | 0       | 0          | 0    | 0     | 4:00 PM     | 0   | 0           | 0           | 0       | 0     |
| 4:05 PM     | 1  | 0   | 8           | 0  | 9     | 4:05 PM     | 0  | 0       | 0          | 0    | 0     | 4:05 PM     | 0   | 0           | 0           | 0       | 0     |
| 4:10 PM     | 3  | 0   | 4           | 0  | 7     | 4:10 PM     | 0  | 0       | 0          | 0    | 0     | 4:10 PM     | 0   | 0           | 0           | 0       | 0     |
| 4:15 PM     | 2  | 0   | 1           | 0  | 3     | 4:15 PM     | 0  | 0       | 0          | 0    | 0     | 4:15 PM     | 0   | 0           | 0           | 0       | 0     |
| 4:20 PM     | 2  | 0   | 3           | 0  | 5     | 4:20 PM     | 0  | 0       | 0          | 0    | 0     | 4:20 PM     | 0   | 1           | 0           | 0       | 1     |
| 4:25 PM     | 3  | 0   | 7           | 0  | 10    | 4:25 PM     | 0  | 0       | 0          | 0    | 0     | 4:25 PM     | 0   | 0           | 0           | 0       | 0     |
| 4:30 PM     | 5  | 0   | 3           | 0  | 8     | 4:30 PM     | 0  | 0       | 0          | 0    | 0     | 4:30 PM     | 0   | 1           | 0           | 0       | 1     |
| 4:35 PM     | 5  | 0   | 3           | 0  | 8     | 4:35 PM     | 0  | 0       | 0          | 0    | 0     | 4:35 PM     | 0   | 0           | 0           | 0       | 0     |
| 4:40 PM     | 4  | 1   | 7           | 0  | 12    | 4:40 PM     | 1  | 0       | 0          | 0    | 1     | 4:40 PM     | 0   | 1           | 0           | 0       | 1     |
| 4:45 PM     | 0  | 0   | 3           | 0  | 3     | 4:45 PM     | 0  | 0       | 0          | 0    | 0     | 4:45 PM     | 0   | 0           | 0           | 0       | 0     |
| 4:50 PM     | 2  | 0   | 3           | 0  | 5     | 4:50 PM     | 0  | 0       | 0          | 0    | 0     | 4:50 PM     | 0   | 0           | 0           | 0       | 0     |
| 4:55 PM     | 3  | 0   | 1           | 0  | 4     | 4:55 PM     | 0  | 0       | 0          | 0    | 0     | 4:55 PM     | 0   | 0           | 0           | 0       | 0     |
| 5:00 PM     | 4  | 0   | 4           | 0  | 8     | 5:00 PM     | 0  | 0       | 0          | 0    | 0     | 5:00 PM     | 0   | 0           | 0           | 0       | 0     |
| 5:05 PM     | 4  | 0   | 1           | 0  | 5     | 5:05 PM     | 0  | 0       | 0          | 0    | 0     | 5:05 PM     | 0   | 0           | 0           | 0       | 0     |
| 5:10 PM     | 2  | 0   | 5           | 0  | 7     | 5:10 PM     | 0  | 0       | 0          | 0    | 0     | 5:10 PM     | 0   | 0           | 0           | 0       | 0     |
| 5:15 PM     | 4  | 0   | 4           | 0  | 8     | 5:15 PM     | 0  | 0       | 1          | 0    | 1     | 5:15 PM     | 0   | 0           | 0           | 0       | 0     |
| 5:20 PM     | 2  | 0   | 5           | 0  | 7     | 5:20 PM     | 0  | 0       | 1          | 0    | 1     | 5:20 PM     | 0   | 0           | 0           | 0       | 0     |
| 5:25 PM     | 5  | 0   | 4           | 0  | 9     | 5:25 PM     | 0  | 0       | 0          | 0    | 0     | 5:25 PM     | 0   | 0           | 0           | 0       | 0     |
| 5:30 PM     | 3  | 0   | 9           | 0  | 12    | 5:30 PM     | 0  | 0       | 0          | 0    | 0     | 5:30 PM     | 0   | 0           | 0           | 0       | 0     |
| 5:35 PM     | 0  | 0   | 4           | 0  | 4     | 5:35 PM     | 0  | 0       | 0          | 0    | 0     | 5:35 PM     | 0   | 0           | 0           | 0       | 0     |
| 5:40 PM     | 4  | 0   | 7           | 0  | 11    | 5:40 PM     | 0  | 0       | 1          | 0    | 1     | 5:40 PM     | 0   | 0           | 0           | 0       | 0     |
| 5:45 PM     | 3  | 0   | 3           | 0  | 6     | 5:45 PM     | 0  | 0       | 1          | 0    | 1     | 5:45 PM     | 0   | 0           | 0           | 0       | 0     |
| 5:50 PM     | 2  | 0   | 3           | 0  | 5     | 5:50 PM     | 0  | 0       | 0          | 0    | 0     | 5:50 PM     | 0   | 0           | 0           | 0       | 0     |
| 5:55 PM     | 4  | 0   | 7           | 0  | 11    | 5:55 PM     | 0  | 0       | 0          | 0    | 0     | 5:55 PM     | 0   | 0           | 0           | 0       | 0     |
| Count Total | 71 | 1   | 102         | 0  | 174   | Count Total | 1  | 0       | 4          | 0    | 5     | Count Total | 0   | 3           | 0           | 0       | 3     |
| Peak Hour   | 33 | 0   | 50          | 0  | 83    | Peak Hour   | 0  | 0       | 3          | 0    | 3     | Peak Hour   | 0   | 0           | 0           | 0       | 0     |

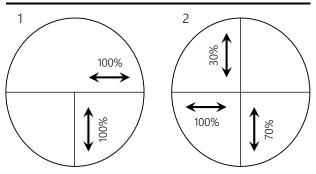




| Trip Generation |  |
|-----------------|--|
|-----------------|--|

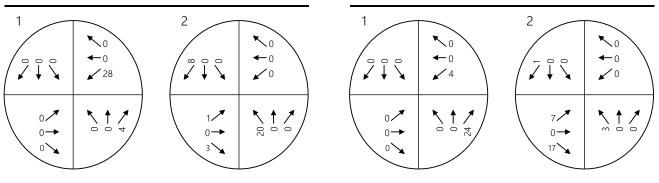
| Period | In  | Out | Total |  |  |
|--------|-----|-----|-------|--|--|
| AM     | 28  | 4   | 32    |  |  |
| PM     | 4   | 24  | 28    |  |  |
| DAILY  | 118 | 118 | 236   |  |  |

Trip Distribution



Site Trip Assignment - AM Peak Hour

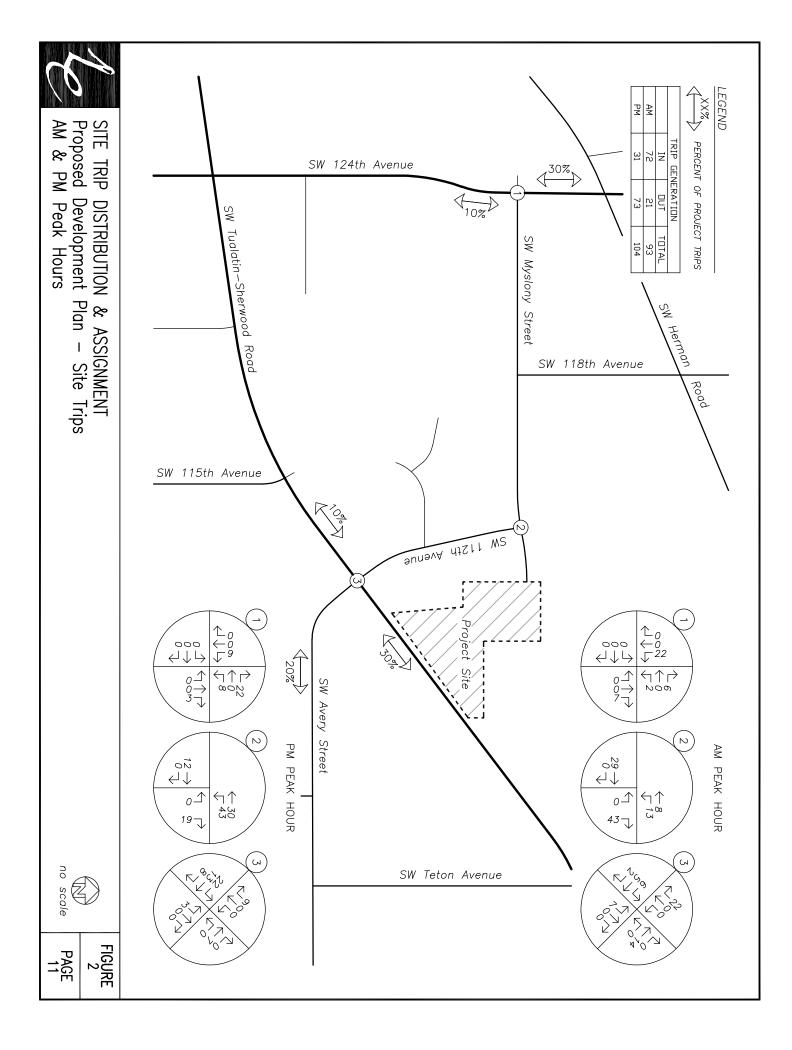
Site Trip Assignment - PM Peak Hour



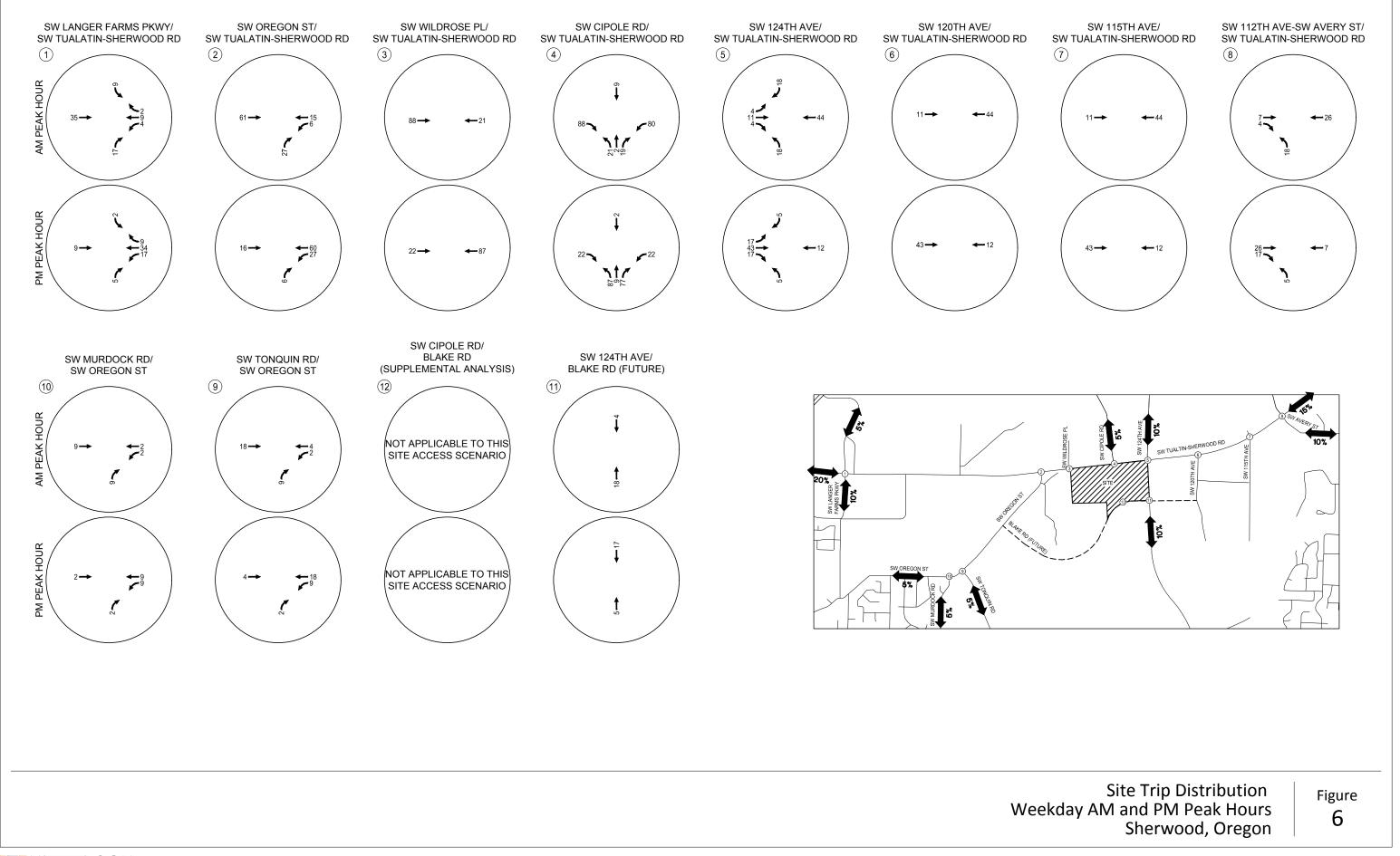


SITE DISTRIBUTION & ASSIGNMENT

Figure 2 10500 SW Manhasset Tualatin



T-S Corporate Park



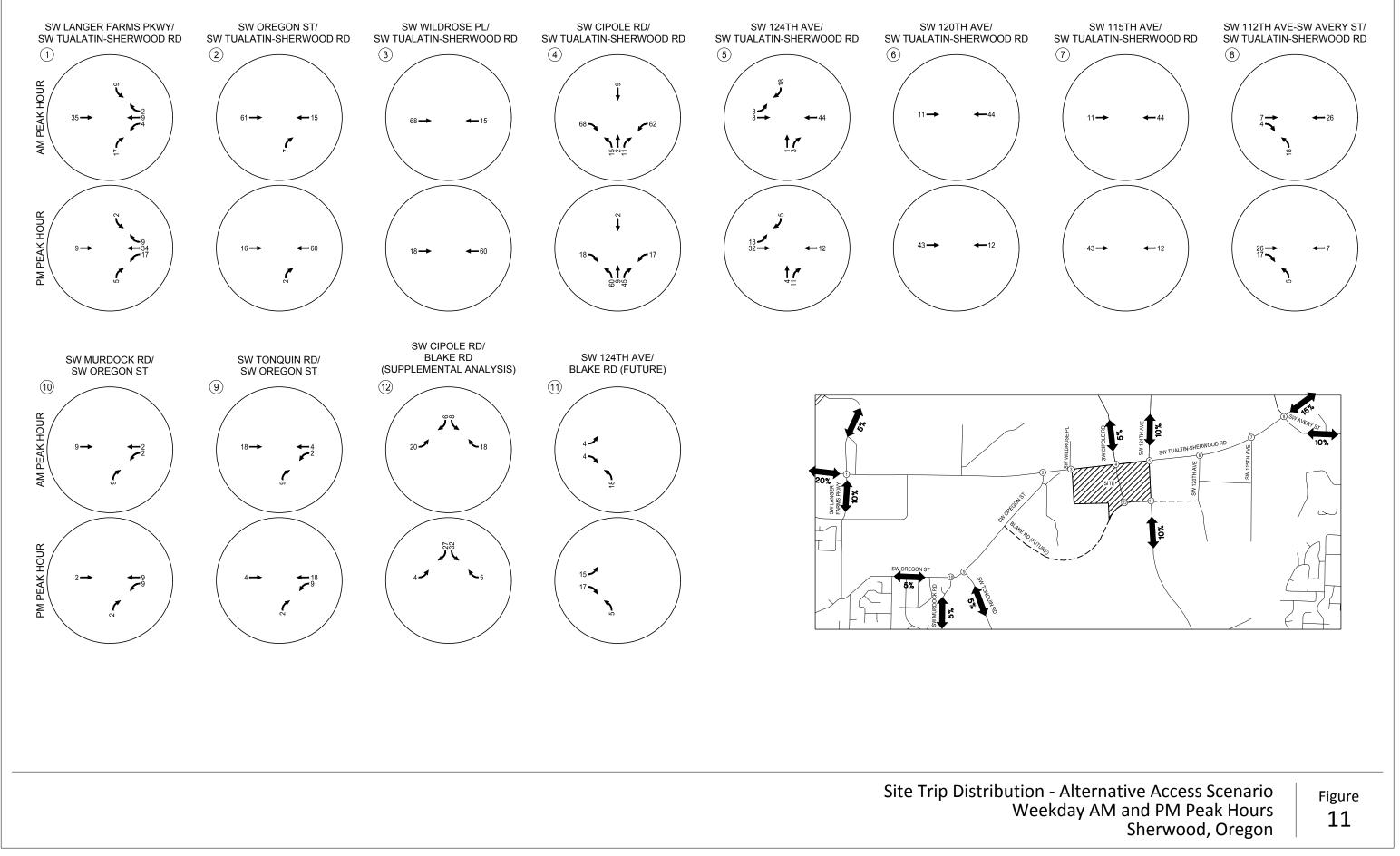


Tab: Trip

1

02.

T-S Corporate Park

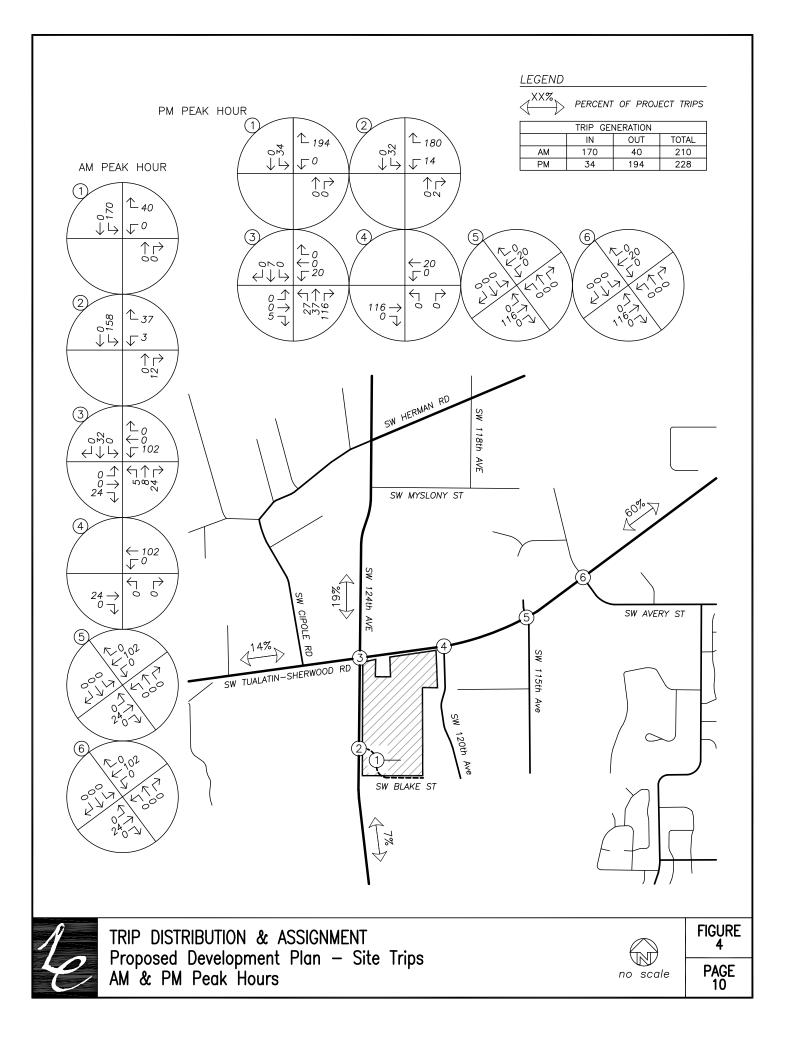




Tab: Trip Dist\_

11

02.



# Appendix C – Safety

Crash Reports

Traffic Signal Warrant Analysis



OREGON.. DEPARTMENT OF TRANSPORTATION - TRANSPORTATION DEVELOPMENT DIVISION

TRANSPORTATION DATA SECTION - CRASH ANAYLYSIS AND REPORTING UNIT

URBAN NON-SYSTEM CRASH LISTING

CITY OF TUALATIN, WASHINGTON COUNTY

TUALATIN-SHERWOOD and Intersectional Crashes at TUALATIN-SHERWOOD, City of Tualatin, Washington County, 01/01/2015 to 12/31/2019

38 - 41 of 605 Crash records shown.

|   | 5  | S D M   |  |   |                      |                                    |                                 |         |                       |                                  |   |  |  |  |                |   |  |  |                 |   |  |
|---|--|---|--|---|----------------------|------------------------------------|---------------------------------|---------|-----------------------|----------------------------------|---|--|--|--|----------------|---|--|--|-----------------|---|--|
| Diame         Diame <th< td=""><td>SER# I</td><td>P R J S W I</td><td>DATE</td><td>CLASS</td><td>CITY STREET</td><td></td><td>INT-TYPE</td><td></td><td></td><td></td><td></td><td>SPCL USE</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>   | SER# I   | P R J S W I   | DATE   | CLASS   | CITY STREET          |                                    | INT-TYPE                        |         |                       |                                  |   | SPCL USE   |  |  |                |   |  |  |                 |   |  |
|   | INVEST E   | EAUICOI   | DAY  | DIST  | FIRST STREET         | RD CHAR                            | (MEDIAN)                        | INT-REL | OFFRD                 | WTHR                             | CRASH                                       | TRLR QTY   | MOVE   |  |                | A                                       | S  |  |                 |   |  |
| C144     N 104     0     104 </td <td>RD DPT H</td> <td>ELGNHRT</td> <td>TIME</td> <td>FROM</td> <td>SECOND STREET</td> <td>DIRECT</td> <td>LEGS</td> <td>TRAF-</td> <td>RNDBT</td> <td>SURF</td> <td>COLL</td> <td>OWNER</td> <td>FROM</td> <td>PRTC</td> <td>INJ</td> <td>G</td> <td>E LI</td> <td>CNS PED</td> <td></td> <td></td> <td></td>   | RD DPT H   | ELGNHRT   | TIME   | FROM  | SECOND STREET        | DIRECT                             | LEGS                            | TRAF-   | RNDBT                 | SURF                             | COLL  | OWNER  | FROM   | PRTC                                     | INJ            | G                                       | E LI   | CNS PED  |                 |   |  |
|   | UNLOC? I   | DCSVLKI   | LAT  | LONG  | LRS                  | LOCTN                              | (#LANES)                        | CONTL   | DRVWY                 | LIGHT                            | SVRTY                                       |  |  | P# TYPE                                  | SVRTY          | E                                       | X RE   | S LOC  | ERROR           | ACT EVENT   | CAUSE  |
| is is is is is is is is is i  |  |   |  |   |                      |                                    |                                 |         |                       |                                  |   |  |  |  |                |   |  |  |                 | 011 013   | 0.0  |
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| <br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br><br>  |  |   |  |   |                      |                                    |                                 |         |                       |                                  |   |  |  |  |                |   |  |  |                 |   |  |
| 1         |  |   |  |   |                      |                                    |                                 |         |                       |                                  |   |  |  |  |                |   |  |  |                 | 022   | 0.0  |
| N         N         N         N         O         N   |  |   |  |   |                      |                                    |                                 |         |                       |                                  |   |  | NE-SW  | 01 DRVR                                  | NONE           | 68                                      | M OR   | -Y   | 000             |   |  |
|   |  |   |  |   |                      |                                    |                                 |         |                       |                                  |   |  |  |  |                |   |  |  |                 |   |  |
| n     i </td <td>03248 1</td> <td>иии и и и и</td> <td>06/24/2019</td> <td>14</td> <td>SW TUALATIN-SHERWOOD</td> <td>STRGHT</td> <td></td> <td>N</td> <td>N</td> <td>CLD</td> <td>S-1STOP</td> <td>01 NONE 0</td> <td>STRGHT</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>07</td>   | 03248 1  | иии и и и и   | 06/24/2019   | 14  | SW TUALATIN-SHERWOOD | STRGHT                             |                                 | N       | N                     | CLD                              | S-1STOP                                     | 01 NONE 0  | STRGHT   |  |                |   |  |  |                 |   | 07   |
| n     i </td <td>CITY</td> <td>Ν</td> <td>MO</td> <td>1300</td> <td>SW AVERY ST</td> <td>NE</td> <td>(NONE)</td> <td>NONE</td> <td>N</td> <td>DRY</td> <td>REAR</td> <td>PRVTE</td> <td>NE-SW</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>000</td> <td>0.0</td>  | CITY   | Ν   | MO   | 1300  | SW AVERY ST          | NE                                 | (NONE)                          | NONE    | N                     | DRY                              | REAR  | PRVTE  | NE-SW  |  |                |   |  |  |                 | 000   | 0.0  |
|   |  |   |  |   |                      |                                    | (                               |         |                       |                                  |   |  |  |  |                |   |  |  |                 |   |  |
| 1/1       1   |  |   |  | -122 47   |                      | 08                                 | (02)                            |         | Ν                     | DAY                              | INJ   | PSNGR CAR  |  | 01 DRVR                                  | NONE           | 16                                      |  |  | 043             | 000   | 07   |
| Aligned   | IN   | -   |  |   |                      |                                    | (02)                            |         |                       |                                  |   |  |  |  |                |   | OR   | ~25  |                 |   |  |
| 2432       8 × 8       9/14/202       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10  |  |   |  |   |                      |                                    |                                 |         |                       |                                  |   |  |  |  |                |   |  |  |                 | 011   | 0.0  |
| Set of the                           |  |   |  |   |                      |                                    |                                 |         |                       |                                  |   |  | NE-SW  | 01 DRVR                                  | TNJC           | 22                                      | FOR  | -Y   | 000             |   |  |
| NNR     57     50    <  |  |   |  |   |                      |                                    |                                 |         |                       |                                  |   |  |  | or prove                                 | 1110 0         |   |  |  |                 |   |  |
| N     52     1,1,1,-1,2,2,7,1     1,2,3,7,1     1,2,3,7,1     1,2,2,4,7,1     1,2,2,4,7,1     1,2,2,4,7,1     1,2,2,4,7,1     1,2,2,4,7,1     1,2,2,4,7,1     1,2,2,4,7,1     1,2,2,4,7,1     1,2,2,4,7,1     1,2,2,4,7,1     1,2,2,4,7,1     1,2,2,4,7,1     1,2,1,4,7,1,4,1,4,1,4,1,4,1,4,1,4,1,4,1,4,1   | 04853  | N N N C   | 09/14/2018   | 14  | SW TUALATIN-SHERWOOD | STRGHT                             |                                 | N       | N                     | CLR                              | S-1TURN                                     | 01 NONE 9  | U-TURN   |  |                |   |  |  |                 |   | 08   |
| N       9       22       3.1 ± 24  | NONE   | F   | FR   | 1500  | SW AVERY ST          | NE                                 | (NONE)                          | UNKNOWN | N                     | DRY                              | TURN  | N/A  | SW-SW  |  |                |   |  |  |                 | 000   | 00   |
| N       9       22       3.1 ± 24  |  |   |  |   |                      |                                    |                                 |         |                       |                                  |   |  |  |  |                |   |  |  |                 |   |  |
| 1     1     3     7 <th>N</th> <th>5</th> <th>5P</th> <th></th> <th></th> <th>07</th> <th></th> <th></th> <th>N</th> <th>DAY</th> <th>PDO</th> <th>PSNGR CAR</th> <th></th> <th>01 DRVR</th> <th>NONE</th> <th>00</th> <th>Unk UN</th> <th>X</th> <th>000</th> <th>000</th> <th>00</th>   | N  | 5   | 5P   |   |                      | 07                                 |                                 |         | N                     | DAY                              | PDO   | PSNGR CAR  |  | 01 DRVR                                  | NONE           | 00                                      | Unk UN   | X  | 000             | 000   | 00   |
| Normal Series in the series of the series       | N<br>N   |   | 45 22 31.14  |   |                      | 07                                 | (02)                            |         | N                     | DAY                              | PDO   | PSNGR CAR  |  | 01 DRVR                                  | NONE           | 00                                      |  |  | 000             | 000   | 00   |
| 0548       N N N       09/20/2017       14       NTALATIN-SHERNOOD       STGHT       Y       N       RAIN       S-STGHT       STGHT   |  |   | 45 22 31.14  |   |                      | 07                                 | (02)                            |         | N                     | DAY                              | PDO   |  | STRGHT   | 01 DRVR                                  | NONE           | 00                                      |  |  | 000             | 000   | 00   |
| No. No.       09/20/2017       14       SM TUALATIN-SHERMOOD       STRGHT       Y       N       RAIN       5-STRGHT       10 NONE       9       STRGHT       STRGHT       10       000  |  |   | 45 22 31.14  |   |                      | 07                                 | (02)                            |         | N                     | DAY                              | PDO   | 02 NONE 9  |  | 01 DRVR                                  | NONE           | 00                                      |  |  | 000             |   |  |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$   |  |   | 45 22 31.14  |   |                      | 07                                 | (02)                            |         | N                     | DAY                              | PDO   | 02 NONE 9<br>N/A   |  |  |                |   | Unk UN   | x<br>x   |                 | 000   | 00   |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$   | N  | 4   | 45 22 31.14  | 15.03   |                      |                                    | (02)                            |         |                       |                                  |   | 02 NONE 9<br>N/A<br>PSNGR CAR  | SW-NE  |  |                |   | Unk UN   | x<br>x   |                 | 000   | 00<br>00   |
| N       45 2 2 1.4 - 1.22 47<br>3.7       45 2 2 1.4 - 1.22 47<br>3.7       (0) <td< td=""><td>N</td><td>4</td><td>45 22 31.14</td><td>15.03</td><td>SW TUALATIN-SHERWOOD</td><td></td><td>(02)</td><td>Ŷ</td><td></td><td></td><td></td><td>02 NONE 9<br/>N/A<br/>PSNGR CAR</td><td>SW-NE</td><td></td><td></td><td></td><td>Unk UN</td><td>x<br/>x</td><td></td><td>000</td><td>00<br/>00</td></td<>  | N  | 4   | 45 22 31.14  | 15.03   | SW TUALATIN-SHERWOOD |                                    | (02)                            | Ŷ       |                       |                                  |   | 02 NONE 9<br>N/A<br>PSNGR CAR  | SW-NE  |  |                |   | Unk UN   | x<br>x   |                 | 000   | 00<br>00   |
| N       45 2 2 1.4 - 1.22 47<br>3.7       45 2 2 1.4 - 1.22 47<br>3.7       (0) <td< td=""><td>N</td><td>4<br/>NNN C</td><td>45 22 31.14<br/>09/20/2017</td><td>15.03</td><td></td><td>STRGHT</td><td></td><td></td><td>N</td><td>RAIN</td><td>S-STRGHT</td><td>02 NONE 9<br/>N/A<br/>PSNGR CAR<br/>01 NONE 9</td><td>SW-NE<br/>STRGHT</td><td></td><td></td><td></td><td>Unk UN</td><td>x<br/>x</td><td></td><td></td><td>00<br/>00<br/>13</td></td<>  | N  | 4<br>NNN C  | 45 22 31.14<br>09/20/2017  | 15.03   |                      | STRGHT                             |                                 |         | N                     | RAIN                             | S-STRGHT                                    | 02 NONE 9<br>N/A<br>PSNGR CAR<br>01 NONE 9   | SW-NE<br>STRGHT  |  |                |   | Unk UN   | x<br>x   |                 |   | 00<br>00<br>13   |
| 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01   | N<br>05848 N   | 4<br>NNN C  | 45 22 31.14<br>09/20/2017<br>WE  | 15.03   |                      | STRGHT                             |                                 |         | N                     | RAIN<br>WET                      | S-STRGHT<br>SS-0                            | 02 NONE 9<br>N/A<br>PSNGR CAR<br>01 NONE 9<br>N/A  | SW-NE<br>STRGHT  | 01 DRVR                                  | NONE           | 00                                      | UN<br>Unk UN<br>UN                                 | χ<br>χ<br>χ  | (000)           | 000<br>000  | 00<br>00<br>13<br>00   |
| NA NA OLIVE SECONDAL     | N<br>05848 N<br>NONE                                   | 4<br>NNN C<br>V<br>4  | 45 22 31.14<br>09/20/2017<br>WE<br>4P<br>45 22 21.49   | 15.03<br>14<br>40<br>-122 47                                |                      | STRGHT                             | (NONE)                          |         | N                     | RAIN<br>WET                      | S-STRGHT<br>SS-0                            | 02 NONE 9<br>N/A<br>PSNGR CAR<br>01 NONE 9<br>N/A  | SW-NE<br>STRGHT  | 01 DRVR                                  | NONE           | 00                                      | Unk UN   | α<br>α<br>α<br>α   | (000)           | 000<br>000  | 00<br>00<br>13<br>00   |
| NOAS       N N N       O2/14/201       14       SW TUALATIN-SHERWOO       STGHT       N       N       C R       S-STGHT       10 NOAS       STGHT       ST       <   | N<br>05848 M<br>NONE<br>N                              | 4<br>NNN C<br>V<br>4  | 45 22 31.14<br>09/20/2017<br>WE<br>4P<br>45 22 21.49   | 15.03<br>14<br>40<br>-122 47                                |                      | STRGHT                             | (NONE)                          |         | N                     | RAIN<br>WET                      | S-STRGHT<br>SS-0                            | 02 NONE 9<br>N/A<br>PSNGR CAR<br>01 NONE 9<br>N/A<br>PSNGR CAR                                       | SW-NE<br>STRGHT<br>SW-NE                                       | 01 DRVR                                  | NONE           | 00                                      | Unk UN   | α<br>α<br>α<br>α   | (000)           | 000<br>000  | 00<br>00<br>13<br>00   |
| 0849       N N       02/14/2015       14       SW TUALATIN-SHERWOO       STGHT       N       N       CLR       S-STRGH       01 NONE       0       STRGH  | N<br>05848 M<br>NONE<br>N                              | 4<br>NNN C<br>V<br>4  | 45 22 31.14<br>09/20/2017<br>WE<br>4P<br>45 22 21.49   | 15.03<br>14<br>40<br>-122 47                                |                      | STRGHT                             | (NONE)                          |         | N                     | RAIN<br>WET                      | S-STRGHT<br>SS-0                            | 02 NONE 9<br>N/A<br>PSNGR CAR<br>01 NONE 9<br>N/A<br>PSNGR CAR<br>02 NONE 9                          | SW-NE<br>STRGHT<br>SW-NE<br>STRGHT                             | 01 DRVR                                  | NONE           | 00                                      | Unk UN   | α<br>α<br>α<br>α   | (000)           | 000<br>000<br>000<br>000  | 00<br>00<br>13<br>00<br>00   |
| NONE     SA     50     SW AVERY ST     SW     (NONE)     UNKNOWN     N     DRY     REAR     PRVE     NE-SW     01     DRV     NONE     45     0.00     000     000       N     10A     10A     122 47     122 47     122 47     122 47     100     00     00     00     00     00     00     00     00     00     00     00     00     00     00     00     00     00     00     0  | N<br>05848 M<br>NONE<br>N                              | 4<br>NNN C<br>V<br>4  | 45 22 31.14<br>09/20/2017<br>WE<br>4P<br>45 22 21.49   | 15.03<br>14<br>40<br>-122 47                                |                      | STRGHT                             | (NONE)                          |         | N                     | RAIN<br>WET                      | S-STRGHT<br>SS-0                            | 02 NONE 9<br>N/A<br>PSNGR CAR<br>01 NONE 9<br>N/A<br>PSNGR CAR                                       | SW-NE<br>STRGHT<br>SW-NE<br>STRGHT                             | 01 DRVR<br>01 DRVR                       | NONE           | 00                                      | Unk UN<br>Unk UN<br>Unk UN                         | α<br>α<br>α<br>α<br>α  | 000             | 000<br>000<br>000<br>000<br>000                                   | 00<br>00<br>13<br>00<br>00<br>00   |
| N 10A 07 N DAY PDO PSNGR CAR 01 DRVR NONE 46 M OR-Y 042 000 29<br>N 45 22 21.43 -122 47<br>32.82 O(2) OR>25 OF CAR OF | N<br>05848 M<br>NONE<br>N<br>N                         | 4<br>NNN (<br>4<br>4  | 45 22 31.14<br>09/20/2017<br>WE<br>4P<br>45 22 21.49   | 15.03<br>14<br>40<br>-122 47                                | SW AVERY ST          | STRGHT<br>SW<br>06                 | (NONE)                          |         | N                     | RAIN<br>WET                      | S-STRGHT<br>SS-0                            | 02 NONE 9<br>N/A<br>PSNGR CAR<br>01 NONE 9<br>N/A<br>PSNGR CAR                                       | SW-NE<br>STRGHT<br>SW-NE<br>STRGHT                             | 01 DRVR<br>01 DRVR                       | NONE           | 00                                      | Unk UN<br>Unk UN<br>Unk UN                         | α<br>α<br>α<br>α<br>α  | 000             | 000<br>000<br>000<br>000<br>000                                   | 00<br>00<br>13<br>00<br>00<br>00   |
| N       45 22 21.43 -122 47<br>32.82       OR>25         02 NONE 0       STRGHT         PRVTE       NE-SW         PSNGR CAR       01 DRVR NONE 34 F       OR>25   | N<br>05848 M<br>NONE<br>N<br>N                         | 4<br>NNN (<br>4<br>4  | 45 22 31.14<br>09/20/2017<br>WE<br>4P<br>45 22 21.49   | 15.03<br>14<br>40<br>-122 47<br>32.7                        | SW AVERY ST          | STRGHT<br>SW<br>06                 | (NONE)                          | UNKNOWN | N<br>N<br>N           | RAIN<br>WET<br>DAY               | S-STRGHT<br>SS-O<br>PDO                     | 02NONE9N/APSNGRCAR01NONE9N/APSNGRCAR02NONE9N/APSNGRCAR   | SW-NE<br>STRGHT<br>SW-NE<br>STRGHT<br>SW-NE                    | 01 DRVR<br>01 DRVR                       | NONE           | 00                                      | Unk UN<br>Unk UN<br>Unk UN                         | α<br>α<br>α<br>α<br>α  | 000             | 000<br>000<br>000<br>000<br>000                                   | 00<br>00<br>13<br>00<br>00<br>00   |
| N       45 22 21.43 -122 47<br>32.82       OR>25         02 NONE 0       STRGHT         PRVTE       NE-SW         PSNGR CAR       01 DRVR NONE 34 F       OR>25   | N<br>05848 M<br>NONE<br>N<br>N                         | 4<br>N N N C<br>4<br>4<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 | 45 22 31.14<br>09/20/2017<br>WE<br>4P<br>45 22 21.49<br>02/14/2015                             | 15.03<br>14<br>40<br>-122 47<br>32.7<br>14                  | SW AVERY ST          | STRGHT<br>SW<br>06<br>STRGHT       | (NONE)<br>(03)                  | UNKNOWN | N<br>N<br>N           | RAIN<br>WET<br>DAY<br>CLR        | S-STRGHT<br>SS-0<br>PDO<br>S-STRGHT         | 02NONE9N/APSNGRCAR01NONE9N/APSNGRCAR02NONE9N/APSNGRCAR01NONE0  | SW-NE<br>STRGHT<br>SW-NE<br>STRGHT<br>SW-NE                    | 01 DRVR<br>01 DRVR                       | NONE           | 00                                      | Unk UN<br>Unk UN<br>Unk UN                         | α<br>α<br>α<br>α<br>α  | 000             | 000<br>000<br>000<br>000<br>000<br>000                            | 00<br>00<br>13<br>00<br>00<br>00<br>00<br>29                               |
| 02       NONE       0       STRGHT       PRVTE       NE-SW       006       00         PSNGR       CAR       01       DRVR       NONE       34       F       OR-Y       000       00   | N<br>05848 M<br>NONE<br>N<br>N<br>N                    | 4<br>NNN C<br>4<br>4<br>4<br>5  | 45 22 31.14<br>09/20/2017<br>WE<br>4P<br>45 22 21.49<br>02/14/2015<br>SA                       | 15.03<br>14<br>40<br>-122 47<br>32.7<br>14                  | SW AVERY ST          | STRGHT<br>SW<br>06<br>STRGHT<br>SW | (NONE)<br>(03)                  | UNKNOWN | N<br>N<br>N<br>N<br>N | RAIN<br>WET<br>DAY<br>CLR<br>DRY | S-STRGHT<br>SS-O<br>PDO<br>S-STRGHT<br>REAR | 02NONE9N/APSNGRCAR01NONE9N/APSNGRCAR02NONE9N/APSNGRCAR01NONE0PRVTEFRVTE                              | SW-NE<br>STRGHT<br>SW-NE<br>STRGHT<br>SW-NE                    | 01 DRVR<br>01 DRVR<br>01 DRVR            | NONE           | 00                                      | Unk UN<br>Unk UN<br>Unk UN<br>Unk UN               | α<br>α<br>α<br>α<br>α<br>α   | 000             | 000<br>000<br>000<br>000<br>000<br>000<br>000                     | 00<br>00<br>13<br>00<br>00<br>00<br>00<br>29<br>00                         |
| PRVTE     NE-SW     006     00       PSNGR CAR     01 DRVR NONE 34 F OR-Y     000     00     00   | N<br>05848 N<br>NONE<br>N<br>N<br>00849 N<br>NONE      | 4<br>NNN C<br>4<br>4<br>4<br>1<br>1   | 45 22 31.14<br>09/20/2017<br>WE<br>4P<br>45 22 21.49<br>02/14/2015<br>SA<br>10A<br>45 22 21.43 | 15.03<br>14<br>40<br>-122 47<br>32.7<br>14<br>50<br>-122 47 | SW AVERY ST          | STRGHT<br>SW<br>06<br>STRGHT<br>SW | ( NONE )<br>( 0 3 )<br>( NONE ) | UNKNOWN | N<br>N<br>N<br>N<br>N | RAIN<br>WET<br>DAY<br>CLR<br>DRY | S-STRGHT<br>SS-O<br>PDO<br>S-STRGHT<br>REAR | 02NONE9N/APSNGRCAR01NONE9N/APSNGRCAR02NONE9N/APSNGRCAR01NONE0PRVTEFRVTE                              | SW-NE<br>STRGHT<br>SW-NE<br>STRGHT<br>SW-NE                    | 01 DRVR<br>01 DRVR<br>01 DRVR            | NONE           | 00                                      | Unk UN<br>Unk UN<br>Unk UN<br>Unk UN<br>M OR       | <b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b> | 000             | 000<br>000<br>000<br>000<br>000<br>000<br>000                     | 00<br>00<br>13<br>00<br>00<br>00<br>00<br>29<br>00                         |
| PSNGR CAR 01 DRVR NONE 34 F OR-Y 000 000 00   | N<br>05848 N<br>NONE<br>N<br>N<br>00849 N<br>NONE<br>N | 4<br>NNN C<br>4<br>4<br>4<br>1<br>1   | 45 22 31.14<br>09/20/2017<br>WE<br>4P<br>45 22 21.49<br>02/14/2015<br>SA<br>10A<br>45 22 21.43 | 15.03<br>14<br>40<br>-122 47<br>32.7<br>14<br>50<br>-122 47 | SW AVERY ST          | STRGHT<br>SW<br>06<br>STRGHT<br>SW | ( NONE )<br>( 0 3 )<br>( NONE ) | UNKNOWN | N<br>N<br>N<br>N<br>N | RAIN<br>WET<br>DAY<br>CLR<br>DRY | S-STRGHT<br>SS-O<br>PDO<br>S-STRGHT<br>REAR | 02NONE9N/APSNGRCAR01NONE9N/APSNGRCAR02NONE9N/APSNGRCAR01NONE0PRVTEPSNGRCAR                           | SW-NE<br>STRGHT<br>SW-NE<br>STRGHT<br>SW-NE<br>STRGHT<br>NE-SW | 01 DRVR<br>01 DRVR<br>01 DRVR            | NONE           | 00                                      | Unk UN<br>Unk UN<br>Unk UN<br>Unk UN<br>M OR       | <b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b> | 000             | 000<br>000<br>000<br>000<br>000<br>000<br>000                     | 00<br>00<br>13<br>00<br>00<br>00<br>00<br>29<br>00                         |
| OR<25   | N<br>05848 N<br>NONE<br>N<br>N<br>00849 N<br>NONE<br>N | 4<br>NNN C<br>4<br>4<br>4<br>1<br>1   | 45 22 31.14<br>09/20/2017<br>WE<br>4P<br>45 22 21.49<br>02/14/2015<br>SA<br>10A<br>45 22 21.43 | 15.03<br>14<br>40<br>-122 47<br>32.7<br>14<br>50<br>-122 47 | SW AVERY ST          | STRGHT<br>SW<br>06<br>STRGHT<br>SW | ( NONE )<br>( 0 3 )<br>( NONE ) | UNKNOWN | N<br>N<br>N<br>N<br>N | RAIN<br>WET<br>DAY<br>CLR<br>DRY | S-STRGHT<br>SS-O<br>PDO<br>S-STRGHT<br>REAR | 02NONE9N/APSNGRCAR01NONE9N/APSNGRCAR02NONE9N/APSNGRCAR01NONE0PRVTEPSNGRCAR02NONE003PRVTEPSNGR04NONE0 | SW-NE<br>STRGHT<br>SW-NE<br>STRGHT<br>SW-NE<br>STRGHT<br>NE-SW | 01 DRVR<br>01 DRVR<br>01 DRVR            | NONE           | 00                                      | Unk UN<br>Unk UN<br>Unk UN<br>Unk UN<br>M OR       | <b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b><br><b>χ</b> | 000             | 000<br>000<br>000<br>000<br>000<br>000<br>000<br>000              | 00<br>00<br>13<br>00<br>00<br>00<br>00<br>29<br>00<br>29                   |
|   | N<br>05848 N<br>NONE<br>N<br>N<br>00849 N<br>NONE<br>N | 4<br>NNN C<br>4<br>4<br>4<br>1<br>1   | 45 22 31.14<br>09/20/2017<br>WE<br>4P<br>45 22 21.49<br>02/14/2015<br>SA<br>10A<br>45 22 21.43 | 15.03<br>14<br>40<br>-122 47<br>32.7<br>14<br>50<br>-122 47 | SW AVERY ST          | STRGHT<br>SW<br>06<br>STRGHT<br>SW | ( NONE )<br>( 0 3 )<br>( NONE ) | UNKNOWN | N<br>N<br>N<br>N<br>N | RAIN<br>WET<br>DAY<br>CLR<br>DRY | S-STRGHT<br>SS-O<br>PDO<br>S-STRGHT<br>REAR | 02NONE9N/APSNGRCAR01NONE9N/APSNGRCAR02NONE9N/APSNGRCAR01NONE0PRVTEPSNGRCAR02NONE0PRVTEPSNGRCAR       | SW-NE<br>STRGHT<br>SW-NE<br>STRGHT<br>SW-NE<br>STRGHT<br>NE-SW | 01 DRVR<br>01 DRVR<br>01 DRVR<br>01 DRVR | NONE NONE NONE | 000000000000000000000000000000000000000 | Unk UN<br>Unk UN<br>Unk UN<br>Unk UN<br>M OR<br>OR | x<br>x<br>x<br>x<br>x<br>x<br>x<br>x<br>x<br>x<br>x<br>x<br>x<br>x<br>x<br>x<br>x<br>x<br>x                          | 000 000 000 000 | 000<br>000<br>000<br>000<br>000<br>000<br>000<br>000<br>000<br>00 | 00<br>00<br>13<br>00<br>00<br>00<br>00<br>29<br>00<br>29<br>00<br>29<br>00 |

Disclaimer: The information contained in this report is compiled from individual driver and police crash report submitted to the Oregon Department of Transportation as required in ORS 811.720. The Crash Analysis and Reporting Unit is committed to providing the highest quality crash data to customers. However, because submitted of crash report forms is the responsibility of the individual driver, the Crash Analysis and Reporting Unit can not guarantee that all details pertaining to a single crash are accurate. Note: Legislative changes to DMV's vehicle crash reporting requirement, effective 01/01/2004, may result in fewer property damage only crashes being eligible for inclusion in the Statewide Crash Data File.

CDS380 02/08/2022

### **Traffic Signal Warrant Analysis**

| Project:<br>Date:<br>Scenario:  | 21175 - Avery I &<br>2/24/2022<br>Year 2023 Buildo |                 |  |                         | 5               |
|---------------------------------|--|-----------------|--|-------------------------|-----------------|
| Major Street:                   | SW Tualatin-She                                    | wood Road       | Minor Street:                                    | Site Access             |                 |
| Number of Lanes:                | 1  |                 | Number of Lanes:                                 | 1                       |                 |
| PM Peak<br>Hour Volumes:        | 1744   |                 | PM Peak<br>Hour Volumes:                         | 89                      |                 |
| Warrant Used:<br>X              | 100 percent of stan                                | dard warrants i | ised   |                         |                 |
|                                 | 70 percent of stand                                | ard warrants us | sed due to 85th perce<br>/ith population less th |                         | ess             |
| Number of                       | Lanes for Moving                                   | ADT or          | n Major St.                                      | ADT on M                | linor St.       |
| Traffic on                      | Each Approach:                                     | (total of bot   | h approaches)                                    | (higher-volum           | e approach)     |
| WARRANT 1, CO                   | NDITION A  | 100%            | 70%  | 100%                    | 70%             |
| <u>Major St.</u>                | <u>Minor St.</u>                                   | <u>Warrants</u> | <u>Warrants</u>                                  | <u>Warrants</u>         | <u>Warrants</u> |
| 1                               | 1  | 8,850           | 6,200  | 2,650                   | 1,850           |
| 2 or more                       | 1  | 10,600          | 7,400  | 2,650                   | 1,850           |
| 2 or more                       | 2 or more  | 10,600          | 7,400  | 3,550                   | 2,500           |
| 1                               | 2 or more  | 8,850           | 6,200  | 3,550                   | 2,500           |
| WARRANT 1, CO                   | NDITION B  |                 |  |                         |                 |
| 1                               | 1  | 13,300          | 9,300  | 1,350                   | 950             |
| 2 or more                       | 1  | 15,900          | 11,100   | 1,350                   | 950             |
| 2 or more                       | 2 or more  | 15,900          | 11,100   | 1,750                   | 1,250           |
| 1                               | 2 or more  | 13,300          | 9,300  | 1,750                   | 1,250           |
|                                 |  | Note: ADT v     | olumes assume 8th high                           | est hour is 5.6% of the | daily volume    |
|                                 |  | Approach        | Minimum  | Is Signal               |                 |
|                                 |  | Volumes         | Volumes  | Warrant Met?            |                 |
| Warrant 1<br>Condition A: Minim | num Vehicular Volume                               | <b>-</b>        |  |                         |                 |
|                                 |  |                 |  |                         |                 |

17,440

890

17,440

890

17,440

890

8,850 2,650

13,300

1,350

10,640

2,120

No

No

No

| * Minor street right-turning | traffic volumes | reduced by 25% |
|------------------------------|-----------------|----------------|
|                              |                 |                |

Condition B: Interruption of Continuous Traffic

Major Street

Minor Street\*

Major Street

Minor Street\*

Combination Warrant

Major Street

Minor Street\*

# Appendix D – Operations Analysis

LOS Data Sheets

Synchro Reports





### Level of Service Definitions

Level of service is used to describe the quality of traffic flow. Levels of service A to C are considered good, and rural roads are usually designed for level of service C. Urban streets and signalized intersections are typically designed for level of service D. Level of service E is considered to be the limit of acceptable delay. For unsignalized intersections, level of service E is generally considered acceptable. Here is a more complete description of levels of service:

- Level of service A: Very low delay at intersections, with all traffic signal cycles clearing and no vehicles waiting through more than one signal cycle. On highways, low volume and high speeds, with speeds not restricted by other vehicles.
- *Level of service B:* Operating speeds beginning to be affected by other traffic; short traffic delays at intersections. Higher average intersection delay than for level of service A resulting from more vehicles stopping.
- *Level of service C:* Operating speeds and maneuverability closely controlled by other traffic; higher delays at intersections than for level of service B due to a significant number of vehicles stopping. Not all signal cycles clear the waiting vehicles. This is the recommended design standard for rural highways.
- Level of service D: Tolerable operating speeds; long traffic delays occur at intersections. The influence of congestion is noticeable. At traffic signals many vehicles stop, and the proportion of vehicles not stopping declines. The number of signal cycle failures, for which vehicles must wait through more than one signal cycle, are noticeable. This is typically the design level for urban signalized intersections.
- Level of service E: Restricted speeds, very long traffic delays at traffic signals, and traffic volumes near capacity. Flow is unstable so that any interruption, no matter how minor, will cause queues to form and service to deteriorate to level of service F. Traffic signal cycle failures are frequent occurrences. For unsignalized intersections, level of service E or better is generally considered acceptable.
- *Level of service F:* Extreme delays, resulting in long queues which may interfere with other traffic movements. There may be stoppages of long duration, and speeds may drop to zero. There may be frequent signal cycle failures. Level of service F will typically result when vehicle arrival rates are greater than capacity. It is considered unacceptable by most drivers.



#### Level of Service Criteria For Signalized Intersections

| Level of Service (LOS) | Control Delay per Vehicle<br>(Seconds) |
|------------------------|--|
| А                      | <10                                    |
| В                      | 10-20                                  |
| С                      | 20-35                                  |
| D                      | 35-55                                  |
| E                      | 55-80                                  |
| F                      | >80                                    |

#### Level of Service Criteria For Unsignalized Intersections

| Level of Service (LOS) | Control Delay per Vehicle<br>(Seconds) |
|------------------------|--|
| А                      | <10                                    |
| В                      | 10-15                                  |
| С                      | 15-25                                  |
| D                      | 25-35                                  |
| E                      | 35-50                                  |
| F                      | >50                                    |

| 02/15/ | 2022 |
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| Intersection           |        |      |      |      |      |          |
|------------------------|--------|------|------|------|------|----------|
| Int Delay, s/veh       | 0.6    |      |      |      |      |          |
| Movement               | NWL    | NWR  | NET  | NER  | SWL  | SWT      |
| Lane Configurations    | ۰¥     |      | 4    |      |      | <b>↑</b> |
| Traffic Vol, veh/h     | 5      | 17   | 652  | 21   | 46   | 667      |
| Future Vol, veh/h      | 5      | 17   | 652  | 21   | 46   | 667      |
| Conflicting Peds, #/hr | 0      | 0    | 0    | 0    | 0    | 0        |
| Sign Control           | Stop   | Stop | Free | Free | Free | Free     |
| RT Channelized         | -      | None | -    | None | -    | None     |
| Storage Length         | 0      | -    | -    | -    | 200  | -        |
| Veh in Median Storage  | e, # 0 | -    | 0    | -    | -    | 0        |
| Grade, %               | 0      | -    | 0    | -    | -    | 0        |
| Peak Hour Factor       | 93     | 93   | 93   | 93   | 93   | 93       |
| Heavy Vehicles, %      | 14     | 14   | 16   | 16   | 11   | 11       |
| Mvmt Flow              | 5      | 18   | 701  | 23   | 49   | 717      |

| Major/Minor          | Minor1 | Ν    | 1ajor1 | Ν | /lajor2 |   |  |
|----------------------|--------|------|--------|---|---------|---|--|
| Conflicting Flow All | 1528   | 713  | 0      | 0 | 724     | 0 |  |
| Stage 1              | 713    | -    | -      | - | -       | - |  |
| Stage 2              | 815    | -    | -      | - | -       | - |  |
| Critical Hdwy        | 6.54   | 6.34 | -      | - | 4.21    | - |  |
| Critical Hdwy Stg 1  | 5.54   | -    | -      | - | -       | - |  |
| Critical Hdwy Stg 2  | 5.54   | -    | -      | - | -       | - |  |
| Follow-up Hdwy       | 3.626  |      | -      | - | 2.299   | - |  |
| Pot Cap-1 Maneuver   | 121    | 412  | -      | - | 839     | - |  |
| Stage 1              | 465    | -    | -      | - | -       | - |  |
| Stage 2              | 415    | -    | -      | - | -       | - |  |
| Platoon blocked, %   |        |      | -      | - |         | - |  |
| Mov Cap-1 Maneuver   | 114    | 412  | -      | - | 839     | - |  |
| Mov Cap-2 Maneuver   | 245    | -    | -      | - | -       | - |  |
| Stage 1              | 465    | -    | -      | - | -       | - |  |
| Stage 2              | 391    | -    | -      | - | -       | - |  |
|                      |        |      |        |   |         |   |  |

| Approach             | NW   | NE | SW  |
|----------------------|------|----|-----|
| HCM Control Delay, s | 15.8 | 0  | 0.6 |
| HCM LOS              | С    |    |     |

| Minor Lane/Major Mvmt | NET | NERNW | /Ln1 | SWL   | SWT |  |
|-----------------------|-----|-------|------|-------|-----|--|
| Capacity (veh/h)      | -   | -     | 357  | 839   | -   |  |
| HCM Lane V/C Ratio    | -   | - 0.  | .066 | 0.059 | -   |  |
| HCM Control Delay (s) | -   | -     | 15.8 | 9.6   | -   |  |
| HCM Lane LOS          | -   | -     | С    | А     | -   |  |
| HCM 95th %tile Q(veh) | -   | -     | 0.2  | 0.2   | -   |  |

| 02/15/ | 2022 |
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| Intersection           |        |      |      |      |      |          |   |
|------------------------|--------|------|------|------|------|----------|---|
| Int Delay, s/veh       | 0.5    |      |      |      |      |          |   |
| Movement               | NWL    | NWR  | NET  | NER  | SWL  | SWT      | • |
| Lane Configurations    | ۰¥     |      | 4    |      |      | <b>↑</b> |   |
| Traffic Vol, veh/h     | 7      | 37   | 802  | 1    | 2    | 679      | ) |
| Future Vol, veh/h      | 7      | 37   | 802  | 1    | 2    | 679      | ) |
| Conflicting Peds, #/hr | 0      | 0    | 0    | 0    | 0    | 0        | ) |
| Sign Control           | Stop   | Stop | Free | Free | Free | Free     | ; |
| RT Channelized         | -      | None | -    | None | -    | None     | ; |
| Storage Length         | 0      | -    | -    | -    | 200  | -        |   |
| Veh in Median Storage  | e, # 0 | -    | 0    | -    | -    | 0        | ) |
| Grade, %               | 0      | -    | 0    | -    | -    | 0        | ) |
| Peak Hour Factor       | 95     | 95   | 95   | 95   | 95   | 95       | ; |
| Heavy Vehicles, %      | 0      | 0    | 4    | 4    | 7    | 7        | , |
| Mvmt Flow              | 7      | 39   | 844  | 1    | 2    | 715      | ; |

| Major/Minor          | Minor1 | M   | ajor1 | Μ   | lajor2 |   |
|----------------------|--------|-----|-------|-----|--------|---|
| Conflicting Flow All | 1564   | 845 | 0     | 0   | 845    | 0 |
| Stage 1              | 845    | -   | -     | -   | -      | - |
| Stage 2              | 719    | -   | -     | -   | -      | - |
| Critical Hdwy        | 6.4    | 6.2 | -     | -   | 4.17   | - |
| Critical Hdwy Stg 1  | 5.4    | -   | -     | -   | -      | - |
| Critical Hdwy Stg 2  | 5.4    | -   | -     | -   | -      | - |
| Follow-up Hdwy       | 3.5    | 3.3 | -     | - 2 | 2.263  | - |
| Pot Cap-1 Maneuver   | 124    | 366 | -     | -   | 771    | - |
| Stage 1              | 425    | -   | -     | -   | -      | - |
| Stage 2              | 486    | -   | -     | -   | -      | - |
| Platoon blocked, %   |        |     | -     | -   |        | - |
| Mov Cap-1 Maneuver   |        | 366 | -     | -   | 771    | - |
| Mov Cap-2 Maneuver   | r 263  | -   | -     | -   | -      | - |
| Stage 1              | 425    | -   | -     | -   | -      | - |
| Stage 2              | 485    | -   | -     | -   | -      | - |
|                      |        |     |       |     |        |   |

| Approach             | NW | NE | SW |
|----------------------|----|----|----|
| HCM Control Delay, s | 17 | 0  | 0  |
| HCM LOS              | С  |    |    |

| Minor Lane/Major Mvmt | NET | NERNWLn1 | SWL   | SWT |  |
|-----------------------|-----|----------|-------|-----|--|
| Capacity (veh/h)      | -   | - 345    | 5 771 | -   |  |
| HCM Lane V/C Ratio    | -   | - 0.134  | 0.003 | -   |  |
| HCM Control Delay (s) | -   | - 17     | 9.7   | -   |  |
| HCM Lane LOS          | -   | - (      | ; А   | -   |  |
| HCM 95th %tile Q(veh) | -   | - 0.5    | 5 0   | -   |  |

| Intersection           |        |      |       |      |      |      |
|------------------------|--------|------|-------|------|------|------|
| Int Delay, s/veh       | 0.5    |      |       |      |      |      |
| Movement               | NWL    | NWR  | NET   | NER  | SWL  | SWT  |
| Lane Configurations    | ۰¥     |      | e î - |      | - ሽ  | ↑    |
| Traffic Vol, veh/h     | 5      | 17   | 713   | 21   | 47   | 842  |
| Future Vol, veh/h      | 5      | 17   | 713   | 21   | 47   | 842  |
| Conflicting Peds, #/hr | 0      | 0    | 0     | 0    | 0    | 0    |
| Sign Control           | Stop   | Stop | Free  | Free | Free | Free |
| RT Channelized         | -      | None | -     | None | -    | None |
| Storage Length         | 0      | -    | -     | -    | 200  | -    |
| Veh in Median Storage  | e, # 0 | -    | 0     | -    | -    | 0    |
| Grade, %               | 0      | -    | 0     | -    | -    | 0    |
| Peak Hour Factor       | 93     | 93   | 93    | 93   | 93   | 93   |
| Heavy Vehicles, %      | 14     | 14   | 16    | 16   | 11   | 11   |
| Mvmt Flow              | 5      | 18   | 767   | 23   | 51   | 905  |

| Major/Minor          | Minor1 | Ν     | /lajor1 | N | /lajor2 |   |  |  |  |  |
|----------------------|--------|-------|---------|---|---------|---|--|--|--|--|
| Conflicting Flow All | 1786   | 779   | 0       | 0 | 790     | 0 |  |  |  |  |
| Stage 1              | 779    | -     | -       | - | -       | - |  |  |  |  |
| Stage 2              | 1007   | -     | -       | - | -       | - |  |  |  |  |
| Critical Hdwy        | 6.54   | 6.34  | -       | - | 4.21    | - |  |  |  |  |
| Critical Hdwy Stg 1  | 5.54   | -     | -       | - | -       | - |  |  |  |  |
| Critical Hdwy Stg 2  | 5.54   | -     | -       | - | -       | - |  |  |  |  |
| Follow-up Hdwy       | 3.626  | 3.426 | -       | - | 2.299   | - |  |  |  |  |
| Pot Cap-1 Maneuver   | 83     | 377   | -       | - | 792     | - |  |  |  |  |
| Stage 1              | 432    | -     | -       | - | -       | - |  |  |  |  |
| Stage 2              | 335    | -     | -       | - | -       | - |  |  |  |  |
| Platoon blocked, %   |        |       | -       | - |         | - |  |  |  |  |
| Mov Cap-1 Maneuver   |        | 377   | -       | - | 792     | - |  |  |  |  |
| Mov Cap-2 Maneuver   | 200    | -     | -       | - | -       | - |  |  |  |  |
| Stage 1              | 432    | -     | -       | - | -       | - |  |  |  |  |
| Stage 2              | 314    | -     | -       | - | -       | - |  |  |  |  |
|                      |        |       |         |   |         |   |  |  |  |  |

| Approach             | NW   | NE | SW  |
|----------------------|------|----|-----|
| HCM Control Delay, s | 17.4 | 0  | 0.5 |
| HCM LOS              | С    |    |     |

| Minor Lane/Major Mvmt | NET | NERNWLn1 | SWL   | SWT | Г |
|-----------------------|-----|----------|-------|-----|---|
| Capacity (veh/h)      | -   | - 314    | 792   | -   | - |
| HCM Lane V/C Ratio    | -   | - 0.075  | 0.064 | -   | - |
| HCM Control Delay (s) | -   | - 17.4   | 9.9   | -   | - |
| HCM Lane LOS          | -   | - C      | A     | -   | - |
| HCM 95th %tile Q(veh) | -   | - 0.2    | 0.2   | -   | - |

| Intersection           |        |      |      |      |      |          |
|------------------------|--------|------|------|------|------|----------|
| Int Delay, s/veh       | 0.5    |      |      |      |      |          |
| Movement               | NWL    | NWR  | NET  | NER  | SWL  | SWT      |
| Lane Configurations    | ۰¥     |      | 4 -  |      |      | <b>↑</b> |
| Traffic Vol, veh/h     | 7      | 38   | 991  | 1    | 2    | 740      |
| Future Vol, veh/h      | 7      | 38   | 991  | 1    | 2    | 740      |
| Conflicting Peds, #/hr | 0      | 0    | 0    | 0    | 0    | 0        |
| Sign Control           | Stop   | Stop | Free | Free | Free | Free     |
| RT Channelized         | -      | None | -    | None | -    | None     |
| Storage Length         | 0      | -    | -    | -    | 200  | -        |
| Veh in Median Storage  | e, # 0 | -    | 0    | -    | -    | 0        |
| Grade, %               | 0      | -    | 0    | -    | -    | 0        |
| Peak Hour Factor       | 95     | 95   | 95   | 95   | 95   | 95       |
| Heavy Vehicles, %      | 0      | 0    | 4    | 4    | 7    | 7        |
| Mvmt Flow              | 7      | 40   | 1043 | 1    | 2    | 779      |

| Major/Minor          | Minor1 | Ν    | 1ajor1 | Ν | /lajor2 |   |
|----------------------|--------|------|--------|---|---------|---|
| Conflicting Flow All | 1827   | 1044 | 0      | 0 | 1044    | 0 |
| Stage 1              | 1044   | -    | -      | - | -       | - |
| Stage 2              | 783    | -    | -      | - | -       | - |
| Critical Hdwy        | 6.4    | 6.2  | -      | - | 4.17    | - |
| Critical Hdwy Stg 1  | 5.4    | -    | -      | - | -       | - |
| Critical Hdwy Stg 2  | 5.4    | -    | -      | - | -       | - |
| Follow-up Hdwy       | 3.5    | 3.3  | -      | - | 2.263   | - |
| Pot Cap-1 Maneuver   |        | 281  | -      | - | 647     | - |
| Stage 1              | 342    | -    | -      | - | -       | - |
| Stage 2              | 454    | -    | -      | - | -       | - |
| Platoon blocked, %   |        |      | -      | - |         | - |
| Mov Cap-1 Maneuver   |        | 281  | -      | - | 647     | - |
| Mov Cap-2 Maneuver   | r 216  | -    | -      | - | -       | - |
| Stage 1              | 342    | -    | -      | - | -       | - |
| Stage 2              | 453    | -    | -      | - | -       | - |
|                      |        |      |        |   |         |   |

| Approach             |      | NE | SW |
|----------------------|------|----|----|
| HCM Control Delay, s | 21.3 | 0  | 0  |
| HCM LOS              | C    | -  | -  |

| Minor Lane/Major Mvmt | NET | NERN\ | NLn1  | SWL   | SWT | - |
|-----------------------|-----|-------|-------|-------|-----|---|
| Capacity (veh/h)      | -   | -     | 268   | 647   | -   | - |
| HCM Lane V/C Ratio    | -   | - (   | 0.177 | 0.003 | -   | - |
| HCM Control Delay (s) | -   | -     | 21.3  | 10.6  | -   | - |
| HCM Lane LOS          | -   | -     | С     | В     | -   | - |
| HCM 95th %tile Q(veh) | -   | -     | 0.6   | 0     | -   | - |

| Intersection           |        |      |      |      |          |      |
|------------------------|--------|------|------|------|----------|------|
| Int Delay, s/veh       | 0.9    |      |      |      |          |      |
| Movement               | NWL    | NWR  | NET  | NER  | SWL      | SWT  |
| Lane Configurations    | ۰¥     |      | eî 👘 |      | <u>ک</u> | •    |
| Traffic Vol, veh/h     | 8      | 24   | 713  | 47   | 94       | 842  |
| Future Vol, veh/h      | 8      | 24   | 713  | 47   | 94       | 842  |
| Conflicting Peds, #/hr | 0      | 0    | 0    | 0    | 0        | 0    |
| Sign Control           | Stop   | Stop | Free | Free | Free     | Free |
| RT Channelized         | -      | None | -    | None | -        | None |
| Storage Length         | 0      | -    | -    | -    | 200      | -    |
| Veh in Median Storage  | e, # 0 | -    | 0    | -    | -        | 0    |
| Grade, %               | 0      | -    | 0    | -    | -        | 0    |
| Peak Hour Factor       | 93     | 93   | 93   | 93   | 93       | 93   |
| Heavy Vehicles, %      | 14     | 14   | 16   | 16   | 11       | 11   |
| Mvmt Flow              | 9      | 26   | 767  | 51   | 101      | 905  |

| Major/Minor          | Minor1   | Ν     | lajor1 | Ν | lajor2 |   |
|----------------------|----------|-------|--------|---|--------|---|
| Conflicting Flow All | 1900     | 793   | 0      | 0 | 818    | 0 |
| Stage 1              | 793      | -     | -      | - | -      | - |
| Stage 2              | 1107     | -     | -      | - | -      | - |
| Critical Hdwy        | 6.54     | 6.34  | -      | - | 4.21   | - |
| Critical Hdwy Stg 1  | 5.54     | -     | -      | - | -      | - |
| Critical Hdwy Stg 2  | 5.54     | -     | -      | - | -      | - |
| Follow-up Hdwy       | 3.626    | 3.426 | -      | - | 2.299  | - |
| Pot Cap-1 Maneuver   | 71       | 370   | -      | - | 772    | - |
| Stage 1              | 425      | -     | -      | - | -      | - |
| Stage 2              | 300      | -     | -      | - | -      | - |
| Platoon blocked, %   |          |       | -      | - |        | - |
| Mov Cap-1 Maneuver   | 62       | 370   | -      | - | 772    | - |
| Mov Cap-2 Maneuver   | 174      | -     | -      | - | -      | - |
| Stage 1              | 425      | -     | -      | - | -      | - |
| Stage 2              | 261      | -     | -      | - | -      | - |
|                      |          |       |        |   |        |   |
| A                    | N IV A / |       |        |   | 014/   |   |

| Approach             | NW   | NE | SW |  |
|----------------------|------|----|----|--|
| HCM Control Delay, s | 19.1 | 0  | 1  |  |
| HCM LOS              | С    |    |    |  |

| Minor Lane/Major Mvmt | NET | NERNW | /Ln1 | SWL   | SWT |
|-----------------------|-----|-------|------|-------|-----|
| Capacity (veh/h)      | -   | -     | 289  | 772   | -   |
| HCM Lane V/C Ratio    | -   | - 0.  | .119 | 0.131 | -   |
| HCM Control Delay (s) | -   | - '   | 19.1 | 10.4  | -   |
| HCM Lane LOS          | -   | -     | С    | В     | -   |
| HCM 95th %tile Q(veh) | -   | -     | 0.4  | 0.5   | -   |

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| Intersection           |        |      |      |      |      |          |   |
|------------------------|--------|------|------|------|------|----------|---|
| Int Delay, s/veh       | 1.8    |      |      |      |      |          |   |
| Movement               | NWL    | NWR  | NET  | NER  | SWL  | SWT      | • |
| Lane Configurations    | ۰¥     |      | - î> |      | - ሽ  | <b>↑</b> |   |
| Traffic Vol, veh/h     | 29     | 79   | 991  | 4    | 9    | 740      | ) |
| Future Vol, veh/h      | 29     | 79   | 991  | 4    | 9    | 740      | ) |
| Conflicting Peds, #/hr | 0      | 0    | 0    | 0    | 0    | 0        | ) |
| Sign Control           | Stop   | Stop | Free | Free | Free | Free     | ; |
| RT Channelized         | -      | None | -    | None | -    | None     | ; |
| Storage Length         | 0      | -    | -    | -    | 200  | -        |   |
| Veh in Median Storage  | e, # 0 | -    | 0    | -    | -    | 0        | ) |
| Grade, %               | 0      | -    | 0    | -    | -    | 0        | ) |
| Peak Hour Factor       | 95     | 95   | 95   | 95   | 95   | 95       | ; |
| Heavy Vehicles, %      | 0      | 0    | 4    | 4    | 7    | 7        | , |
| Mvmt Flow              | 31     | 83   | 1043 | 4    | 9    | 779      | ) |

| Major/Minor          | Minor1 | Ν    | lajor1 | Ν | lajor2 |   |
|----------------------|--------|------|--------|---|--------|---|
| Conflicting Flow All | 1842   | 1045 | 0      | 0 | 1047   | 0 |
| Stage 1              | 1045   | -    | -      | - | -      | - |
| Stage 2              | 797    | -    | -      | - | -      | - |
| Critical Hdwy        | 6.4    | 6.2  | -      | - | 4.17   | - |
| Critical Hdwy Stg 1  | 5.4    | -    | -      | - | -      | - |
| Critical Hdwy Stg 2  | 5.4    | -    | -      | - | -      | - |
| Follow-up Hdwy       | 3.5    | 3.3  | -      | - | 2.263  | - |
| Pot Cap-1 Maneuver   | 84     | 280  | -      | - | 646    | - |
| Stage 1              | 342    | -    | -      | - | -      | - |
| Stage 2              | 447    | -    | -      | - | -      | - |
| Platoon blocked, %   |        |      | -      | - |        | - |
| Mov Cap-1 Maneuver   | r 83   | 280  | -      | - | 646    | - |
| Mov Cap-2 Maneuver   | r 213  | -    | -      | - | -      | - |
| Stage 1              | 342    | -    | -      | - | -      | - |
| Stage 2              | 441    | -    | -      | - | -      | - |
|                      |        |      |        |   |        |   |
|                      |        |      |        |   |        |   |

| Approach             | NW   | NE | SW  |
|----------------------|------|----|-----|
| HCM Control Delay, s | 29.5 | 0  | 0.1 |
| HCM LOS              | D    |    |     |

| Minor Lane/Major Mvmt | NET | NERN | WLn1  | SWL   | SWT | • |
|-----------------------|-----|------|-------|-------|-----|---|
| Capacity (veh/h)      | -   | -    | 258   | 646   | -   | - |
| HCM Lane V/C Ratio    | -   | -    | 0.441 | 0.015 | -   | - |
| HCM Control Delay (s) | -   | -    | 29.5  | 10.7  | -   | - |
| HCM Lane LOS          | -   | -    | D     | В     | -   | - |
| HCM 95th %tile Q(veh) | -   | -    | 2.1   | 0     | -   |   |

| Intersection           |        |      |             |      |      |          |   |
|------------------------|--------|------|-------------|------|------|----------|---|
| Int Delay, s/veh       | 0.9    |      |             |      |      |          |   |
| Movement               | NWL    | NWR  | NET         | NER  | SWL  | SWT      |   |
| Lane Configurations    | ۰¥     |      | <b>∱</b> î≽ |      | - ከ  | <b>^</b> |   |
| Traffic Vol, veh/h     | 8      | 24   | 713         | 47   | 94   | 842      | 2 |
| Future Vol, veh/h      | 8      | 24   | 713         | 47   | 94   | 842      | 2 |
| Conflicting Peds, #/hr | 0      | 0    | 0           | 0    | 0    | 0        | ) |
| Sign Control           | Stop   | Stop | Free        | Free | Free | Free     | ; |
| RT Channelized         | -      | None | -           | None | -    | None     | ; |
| Storage Length         | 0      | -    | -           | -    | 200  | -        | - |
| Veh in Median Storage  | e, # 0 | -    | 0           | -    | -    | 0        | ) |
| Grade, %               | 0      | -    | 0           | -    | -    | 0        | ) |
| Peak Hour Factor       | 93     | 93   | 93          | 93   | 93   | 93       | 3 |
| Heavy Vehicles, %      | 14     | 14   | 16          | 16   | 11   | 11       |   |
| Mvmt Flow              | 9      | 26   | 767         | 51   | 101  | 905      | 5 |

| Major/Minor          | Minor1 | Μ    | lajor1 | Ν | lajor2 |   |
|----------------------|--------|------|--------|---|--------|---|
| Conflicting Flow All | 1448   | 409  | 0      | 0 | 818    | 0 |
| Stage 1              | 793    | -    | -      | - | -      | - |
| Stage 2              | 655    | -    | -      | - | -      | - |
| Critical Hdwy        | 7.08   | 7.18 | -      | - | 4.32   | - |
| Critical Hdwy Stg 1  | 6.08   | -    | -      | - | -      | - |
| Critical Hdwy Stg 2  | 6.08   | -    | -      | - | -      | - |
| Follow-up Hdwy       | 3.64   | 3.44 | -      | - | 2.31   | - |
| Pot Cap-1 Maneuver   | 109    | 559  | -      | - | 751    | - |
| Stage 1              | 377    | -    | -      | - | -      | - |
| Stage 2              | 447    | -    | -      | - | -      | - |
| Platoon blocked, %   |        |      | -      | - |        | - |
| Mov Cap-1 Maneuver   | · 94   | 559  | -      | - | 751    | - |
| Mov Cap-2 Maneuver   | · 217  | -    | -      | - | -      | - |
| Stage 1              | 377    | -    | -      | - | -      | - |
| Stage 2              | 387    | -    | -      | - | -      | - |
|                      |        |      |        |   |        |   |
| Approach             | NW     |      | NE     |   | SW     |   |

| Approach             | NW   | NE | SW  |  |
|----------------------|------|----|-----|--|
| HCM Control Delay, s | 14.8 | 0  | 1.1 |  |
| HCM LOS              | В    |    |     |  |

| Minor Lane/Major Mvmt | NET | NERNWLn1 | SWL   | SWT |  |
|-----------------------|-----|----------|-------|-----|--|
| Capacity (veh/h)      | -   | - 401    | 751   | -   |  |
| HCM Lane V/C Ratio    | -   | - 0.086  | 0.135 | -   |  |
| HCM Control Delay (s) | -   | - 14.8   | 10.5  | -   |  |
| HCM Lane LOS          | -   | - E      | В     | -   |  |
| HCM 95th %tile Q(veh) | -   | - 0.3    | 0.5   | -   |  |

#### Intersection

| Int Delay, s/veh       | 1.1   |      |               |      |      |      |
|------------------------|-------|------|---------------|------|------|------|
| Movement               | NWL   | NWR  | NET           | NER  | SWL  | SWT  |
| Lane Configurations    | Y     |      | _ <b>≜</b> î≽ |      | ٦    | - 11 |
| Traffic Vol, veh/h     | 29    | 79   | 991           | 4    | 9    | 740  |
| Future Vol, veh/h      | 29    | 79   | 991           | 4    | 9    | 740  |
| Conflicting Peds, #/hr | 0     | 0    | 0             | 0    | 0    | 0    |
| Sign Control           | Stop  | Stop | Free          | Free | Free | Free |
| RT Channelized         | -     | None | -             | None | -    | None |
| Storage Length         | 0     | -    | -             | -    | 200  | -    |
| Veh in Median Storage  | , # 0 | -    | 0             | -    | -    | 0    |
| Grade, %               | 0     | -    | 0             | -    | -    | 0    |
| Peak Hour Factor       | 95    | 95   | 95            | 95   | 95   | 95   |
| Heavy Vehicles, %      | 0     | 0    | 4             | 4    | 7    | 7    |
| Mvmt Flow              | 31    | 83   | 1043          | 4    | 9    | 779  |

| Major/Minor          | Minor1 | М   | ajor1 | Ν | /lajor2 |   |  |
|----------------------|--------|-----|-------|---|---------|---|--|
| Conflicting Flow All | 1453   | 524 | 0     | 0 | 1047    | 0 |  |
| Stage 1              | 1045   | -   | -     | - | -       | - |  |
| Stage 2              | 408    | -   | -     | - | -       | - |  |
| Critical Hdwy        | 6.8    | 6.9 | -     | - | 4.24    | - |  |
| Critical Hdwy Stg 1  | 5.8    | -   | -     | - | -       | - |  |
| Critical Hdwy Stg 2  | 5.8    | -   | -     | - | -       | - |  |
| Follow-up Hdwy       | 3.5    | 3.3 | -     | - | 2.27    | - |  |
| Pot Cap-1 Maneuver   | 123    | 503 | -     | - | 631     | - |  |
| Stage 1              | 304    | -   | -     | - | -       | - |  |
| Stage 2              | 646    | -   | -     | - | -       | - |  |
| Platoon blocked, %   |        |     | -     | - |         | - |  |
| Mov Cap-1 Maneuver   | · 121  | 503 | -     | - | 631     | - |  |
| Mov Cap-2 Maneuver   | 234    | -   | -     | - | -       | - |  |
| Stage 1              | 304    | -   | -     | - | -       | - |  |
| Stage 2              | 637    | -   | -     | - | -       | - |  |
|                      |        |     |       |   |         |   |  |

| Minor Lane/Major Mvmt | NET | NERN | WLn1  | SWL   | SWT |
|-----------------------|-----|------|-------|-------|-----|
| Capacity (veh/h)      | -   | -    | 384   | 631   | -   |
| HCM Lane V/C Ratio    | -   | -    | 0.296 | 0.015 | -   |
| HCM Control Delay (s) | -   | -    | 18.3  | 10.8  | -   |
| HCM Lane LOS          | -   | -    | С     | В     | -   |
| HCM 95th %tile Q(veh) | -   | -    | 1.2   | 0     | -   |