## (LI) lancaster mobley



EXPIRATION DATE: $6 / 30 / 2022$

## Avery I and II

## Transportation Impact

 Analysis
## Tualatin, Oregon

Date:
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## Executive Summary

1. The proposed development at 10500/10700 SW Tualatin-Sherwood Road includes the construction of two industrial buildings totaling approximately 112,500 square feet. Construction is expected to be completed with occupancy beginning in the year 2023.
2. The proposed development is estimated to generate 83 morning peak hour, 73 evening peak hour, and 548 average weekday trips.
3. Based on a review of the available crash data and crash rates, patterns are consistent with the geometry and traffic control provided at the study intersection. The proposed project is not expected to change or worsen crash rates. Accordingly, no safety mitigation is recommended per the crash data analysis.
4. Preliminary traffic signal warrants are not met at any of the unsignalized study area intersections under buildout conditions.
5. The study intersection is currently operating acceptably per Washington County standards and is projected to continue operating acceptably through the 2023 buildout year of the site. No operational mitigation is required or recommended.
6. The construction of the planned five lane cross-section on SW Tualatin-Sherwood Road will not adversely affect future operations at the study intersection.

## Introduction

The proposed development at 10500/10700 SW Tualatin-Sherwood Road includes the construction of two industrial buildings totaling approximately 112,500 square feet. Construction is expected to be completed with occupancy beginning in the year 2023.

Based on correspondence with the City of Tualatin staff, the study area includes one intersection:

- Site Access at SW Tualatin-Sherwood Road

This report examines the impacts of the proposed development on the transportation system in the vicinity of the project site. The purpose of this study is to analyze potential traffic impacts and recommend any required transportation mitigation measures to ensure safe and efficient performance of the transportation facilities that will be impacted by the proposed development. In addition to the operational analysis, the report includes a safety analysis at the study intersection.

Detailed information on traffic counts, trip generation calculations, safety analyses, and operations are included in the appendices to this report.

## Location Description

The project site is located south of SW Tualatin-Sherwood Road, north of SW Avery Street, and west of SW Teton Avenue in Tualatin, Oregon. The proposed development includes the construction of two warehouse buildings totaling approximately 112,525 square feet on two tax lots (tax lots 2S126B00105 and 2S127AA02100). Both parcels are zoned General Manufacturing (MG) and are centrally located within Tualatin's industrially zoned lands.

The Avery I site is located at 10700 SW Tualatin-Sherwood Road and will house an 81,075 square-foot warehouse. The Avery II site is located at 10500 SW Tualatin-Sherwood Road and will house a 31,050 squarefoot warehouse. Both sites will take access from SW Tualatin-Sherwood Road via an existing shared driveway.

An aerial view of the proposed site and the nearby vicinity is displayed in Figure 1, with the subject sites outlined in yellow. A site plan is included in Appendix A.


Figure 1: Project Location (image from Google Maps)

## Vicinity Roadways

The proposed development is expected to impact two major roadways near the site. Table 1 provides a description of each of the vicinity roadways.

Table 1: Vicinity Roadway Descriptions

| Roadway | Classification | Jurisdiction | Travel Lanes | Speed (mph) | Curbs | Sidewalks | Bicycle <br> Lanes | On-Street Parking |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SW TualatinSherwood Road | Major <br> Arterial | Washington County | 3-5 | $45$ <br> (Posted) | Both <br> Sides | Both Sides | Both <br> Sides | Not Permitted |
| SW Teton Avenue | Minor <br> Arterial | City of Tualatin | 3 | 35 <br> (Posted) | Both Sides | Both Sides w/ Exceptions ${ }^{1}$ | None | Not Permitted |

## Notes:

1. Sidewalk is missing on west side of SW Teton Avenue where adjacent land is undeveloped between SW Tualatin-Sherwood Road and SW Manhasset Drive.

## Study Intersections

Through coordination with the City of Tualatin and Washington County, one study intersection was identified for analysis. A summarized description of the study intersection is provided in Table 2.

Table 2: Study Intersection Descriptions

| Intersection |  | Geometry | Traffic Control | Phasing/Stopped Approaches |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Site Access (Existing) at <br> SW Tualatin-Sherwood Road | Three-Legged | Stop-Controlled | NB Stop-Controlled |

## Public Transit

The project is located near one transit line that has stops within an approximate one-half mile walking/biking distance from the site.

Bus Line \# 97 - Tualatin-Sherwood Road provides weekday rush-hour service between W Langer Drive/Sherwood Plaza and the Tualatin WES Station. The nearest bus stops to the site are located at the intersection of SW Teton Avenue and SW Tualatin-Sherwood Road. Weekday service is scheduled with four westbound and three eastbound trips in the morning at approximately 60 -minute headways. Afternoon service is scheduled with four eastbound and three westbound trips at approximately 60 -minute headways. There is currently no weekend or holiday service.

A vicinity map showing the project site, vicinity streets, and study intersection configuration is shown in Figure 2.STUDY INTERSECTION

- STOP SIGN
\& BIKE LANE
$\triangle$ PROJECT SITE
- ARTERIAL ROADWAY
- COLLECTOR ROADWAY
- LOCAL ROADWAY


Figure 2

## Site Trips

## Trip Generation

To estimate trips that will be generated by the proposed development, trip rates from the Trip Generation Manual ${ }^{1}$ were used. Based on direction from City of Tualatin staff, data from land-use code 110 (General Light Industrial) was used to estimate the proposed development's trip generation based on square footage of gross floor area. The client has indicated that both buildings in the proposed development will be used for the storage and distribution of materials.

The trip generation calculations show that the proposed development is projected to generate 83 trips during the morning peak hour, 73 trips during the evening peak hour, and 548 trips during the average weekday. The trip generation estimates are summarized in Table 3. Detailed trip generation calculations are included in Appendix A.

Table 3: Trip Generation Summary

| Land Use | ITE <br> Code | Size/Rate | Moming Peak Hour |  |  | Evening Peak Hour |  |  | Weekday <br> Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out | Total | In | Out | Total |  |
| General Light Industrial | 110 | 112,525 | 73 | 10 | 83 | 10 | 63 | 73 | 548 |

Given that the surrounding site vicinity is primarily industrial in character, the nearby transportation system was constructed to serve the needs of existing and future industrial development. As such, it is expected that a majority of trips would utilize the transportation corridors of SW Tualatin-Sherwood Road and SW Teton Avenue. From SW Tualatin-Sherwood Road and SW Teton Avenue, access to regional transportation facilities, such as SW Pacific Highway, SW Boones Ferry Road (OR-141), Interstate 5, and Interstate 205, are available.

## Trip Distribution

The following trip distribution was estimated based on existing traffic volumes, the locations of likely trip destinations, and locations of major transportation facilities in the site vicinity:

- Approximately 45 percent of site trips will travel to/from the east along SW Tualatin-Sherwood Road;
- Approximately 35 percent of site trips will travel to/from the west along SW Tualatin-Sherwood Road;
- Approximately 10 percent of site trips will travel to/from the north along SW Teton Avenue; and
- Approximately 10 percent of site trips will travel to/from the south along SW Teton Avenue.

Staff provided a general guideline of 60 peak hour trips and 500 daily trips through an intersection during the scoping phase for a previous project (Tualatin Logistics Traffic Study Scoping Memorandum - Revised, June 18,

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2021). Washington County (Resolution \& Order 86-95) defines the impact area for developments as "those road links where site-generated traffic equals or exceeds $10 \%$ of existing average daily traffic" (ADT).

Table 4 summarizes the estimated number of additional trips through nearby intersections based on the trip distribution described above. No intersections are expected to have more additional trips than the 60 peak hour trip threshold or be over the 500 daily trip threshold.

Table 4: Additional Peak Hour and Weekday Trips Summary

| Intersection | Site Trip <br> Distribution | Net Site Trips <br> Peak Hour |  |
| :---: | :---: | :---: | :---: |
| SW 124 $4^{\text {th }}$ Avenue \& SW Tualatin-Sherwood Road | $35 \%$ | 29 | 192 |
| SW 112 ${ }^{\text {th }}$ Avenue/SW Avery Street \& SW Tualatin-Sherwood Road | $35 \%$ | 29 | 192 |
| SW Teton Avenue \& SW Tualatin-Sherwood Road | $65 \%$ | 54 | 356 |
| SW Boones Ferry Road at SW Tualatin-Sherwood Road | $45 \%$ | 37 | 247 |

Traffic data from the Oregon Department of Transportation's (ODOT) TransGIS website was reviewed to determine where daily site trips are anticipated to exceed ten percent of the existing ADT and identify intersections to be analyzed in the TIA. Table 5 summarizes the ADT on roadways within the site vicinity and the estimated site trips on the subject roadways.

Table 5: Weekday Site Trips and Existing ADT Summary

| Roadway | Point | Site Trip Distribution | Site Trips | Existing ADT | Ratio of Site Trips to Existing ADT (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SW TualatinSherwood Road | East of SW $124^{\text {th }}$ Avenue, west of SW $120^{\text {th }}$ Avenue | 35\% | 192 | 29,900 | 0.6\% |
| SW TualatinSherwood Road | 0.01 mile west of SW Boones Ferry Road | 45\% | 247 | 34,300 | 0.7\% |

Note: Existing ADT based on ODOT TransGIS Traffic Data

Considering the net increase in traffic on area roadways, none of the nearby intersections or roadways are anticipated to sustain a significant increase in traffic volume or meet the volume threshold guidelines provided by Staff. Therefore, no off-site intersections are proposed for analysis as part of this report.

The trip distribution and assignment for the total site trips generated during the morning and evening peak hours is shown in Figure 3.
LEGEND

| $X X \%$ |  |  |  |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| TRIP GENERATION PERCENT OF PROJECT TRIPS |  |  |  |
|  | IN | OUT | TOTAL |
| AM | 73 | 10 | 83 |
| PM | 10 | 63 | 73 |

AM PEAK HOUR PM PEAK HOUR


## Traffic Volumes

## Existing Conditions

Traffic counts were conducted at the study intersection on Thursday, February 10, 2022, from 7:00 AM to 9:00 AM and from 4:00 PM to 6:00 PM. Data was used from the intersection's respective morning and evening peak hours. Raw count data is included in Appendix B.

The ongoing COVID-19 viral pandemic, which began in March 2020, has initiated a significant decrease in traffic due to policies on social distancing that have closed or limited business operations and reduced commuting as many people work from home. A comparison of the Portland State University (PSU) Portal data for the l-5 interchange on-ramps near the project site shows that most volumes are at most about 1 percent lower at the end of October 2021 as compared with the same period in 2019. As a result, new traffic data collected for this project was not adjusted for "normal" conditions, as current traffic volumes are close to pre-COVID volumes.

Figure 4 shows the existing traffic volumes at the study intersection for the morning and evening peak hours.

## Background Conditions

To provide analysis of the impact of the proposed development on the nearby transportation facilities, an estimate of future traffic volumes is required. A compounded growth rate of two percent per year for an assumed buildout condition of one year was applied to the measured existing traffic volumes to approximate general growth for year 2023 background conditions.

In addition to the traffic volume growth described above, trips associated with two in-process developments within the site vicinity ${ }^{2}$, that are currently approved but not yet fully constructed or occupied, were added to the existing volumes in addition to the calculated volume growth. The following projects were assumed to be completed and occupied prior to year 2023:

- PGE Integrated Operations Center;
- Sherwood Industrial Park;
- Manhasset Industrial ( 10500 SW Manhasset Drive); and
- Tualatin Industrial Park (11045 SW Tualatin-Sherwood Road)

Figures depicting trip assignment associated with the in-process developments are included in Appendix B. Figure 5 shows the projected year 2023 background volumes at the study intersection for the morning and evening peak hours.

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## Buildout Conditions

The trips estimated to be generated by the proposed development, as described earlier within the Site Trips section, were added to the year 2023 background traffic volumes to estimate traffic volumes under the year 2023 buildout conditions.

Figure 6 shows the projected year 2023 buildout volumes at the study intersection for the morning and evening peak hours.

## Future Roadway Improvements

Improvements along Tualatin-Sherwood Road (between Teton Avenue and Langer Farms Parkway) are planned to begin in 2022 and finish by 2025. As part of this project, the roadway will be widened to five travel lanes (two travel lanes in each direction and a center-turn lane) and bicycle and pedestrian facilities will be included along both sides of the roadway.
AM PEAK HOUR PM PEAK HOUR


TRAFFIC VOLUMES
Year 2022 Existing Conditions
AM \& PM Peak Hours

Figure 4
Avery I \& II
2/15/2022


TRAFFIC VOLUMES
Year 2023 Background Conditions
AM \& PM Peak Hours

Figure 5
Avery I \& II
2/15/2022


TRAFFIC VOLUMES
Year 2023 Buildout Conditions
AM \& PM Peak Hours

Figure 6
Avery I \& II
2/15/2022

## Safety Analysis

## Crash History Review

Using data obtained from the ODOT's Crash Data System, the most recent available five years of crash history (January 2015 to December 2019) at the study intersection was reviewed. The crash data were evaluated based on the number of crashes, the type of collisions, the severity of the collisions, and the resulting crash rate for the intersection.

Crash severity is based on injuries sustained by people involved in the crash. ODOT classifies crash severity into the following five categories:

- Property Damage Only (PDO)
- Possible Injury (Injury C)
- Non-Incapacitating Injury (Injury B)
- Incapacitating Injury (Injury A)
- Fatality or Fatal Injury

Crash rates provide the ability to compare safety risks at different intersections by accounting for both the number of crashes that have occurred during the study period and the number of vehicles that typically travel through the intersection. Crash rates were calculated using the common assumption that traffic counted during the evening peak period represents approximately 10 percent of the annual average daily traffic (AADT) at the intersection.

Table 6 provides a summary of collision types, crash severities, and the calculated crash rate for the study intersection. Detailed ODOT crash reports are included in Appendix C.

Table 6: Crash Type Summary

| Intersection |  | Collision Type |  | Crash Severity |  |  |  |  | Total Crashes | AADT | Crash Rate |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Turn | Other | PDO | c | B | A | Fatal |  |  |  |
| 1 | Site Access at SW TualatinSherwood Road | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 15,280 | 0.036 |

Based on a review of the available crash data and crash rates, patterns are consistent with the geometry and traffic control provided at the study intersection. The proposed project is not expected to change or worsen crash rates. Accordingly, no safety mitigation is recommended per the crash data analysis.

## Warrant Analysis

Left-turn lane warrants and preliminary traffic signal warrants were examined for the study intersection where such treatments would be applicable.

## Left-Turn Lane Warrants

Left-turn lane warrants were not examined for the westbound approach from SW Tualatin-Sherwood Road into the site as the roadway has an existing two-way left-turn lane as part of the roadway cross-section.

## Preliminary Traffic Signal Warrants

Preliminary traffic signal warrants were examined at the site access intersection to determine whether the installation of a new traffic signal will be warranted at this intersection upon completion of the proposed development.

Traffic signal warrants are not met this intersection under buildout conditions. Detailed information on the warrant analysis is included in Appendix C.

## Sight Distance

Sight distance was not measured and evaluated, as the proposed development will be using an existing access

## Operational Analysis

A capacity and delay analysis was conducted for the study intersection per the unsignalized intersection analysis methodologies in the Highway Capacity Manual (HCM) $6^{\text {th }}$ Edition ${ }^{3}$. Intersections are generally evaluated based on the average control delay experienced by vehicles and are assigned a grade according to their operation. The level of service (LOS) of an intersection can range from LOS A, which indicates very little or no delay experienced by vehicles, to LOS F, which indicates a high degree of congestion and delay. The volume-tocapacity ( $\mathrm{v} / \mathrm{c}$ ) ratio is a measure that compares the traffic volumes (demand) against the available capacity of an intersection.

## Performance Standards

Intersections along SW Tualatin-Sherwood Road are under the jurisdiction of Washington County, where the County requires intersections to operate with a v/c ratio of 0.99 or less.

## Delay \& Capacity Analysis

The LOS, delay, and $\mathrm{v} / \mathrm{c}$ results of the capacity analysis are shown in Table 7. Detailed calculations as well as tables showing the relationship between delay and LOS are included in Appendix D.

[^2]Table 7: Intersection Capacity Analysis Summary

| Condition | Morning Peak Hour |  |  | Evening Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay (s) | v/c | LOS | Delay (s) | $\mathrm{v} / \mathrm{c}$ |
| 1. Site Access (Existing) at SW Tualatin-Sherwood Road |  |  |  |  |  |  |
| 2021 Existing Condition | C | 16 | 0.07 | C | 17 | 0.13 |
| 2023 Background Condition | C | 17 | 0.08 | C | 21 | 0.18 |
| 2023 Buildout Condition | C | 19 | 0.13 | D | 30 | 0.44 |

The study intersection is currently operating acceptably per Washington County standards and is projected to continue operating acceptably through the 2023 buildout year of the site. No operational mitigation is required or recommended.

This project will be completed prior to the construction of the planned five lane cross-section on SW TualatinSherwood Road. However, a review of operations with the future configuration shows that operations are not adversely impacted at the site driveway when the widening of SW Tualatin-Sherwood Road is completed.

## Conclusions

Key findings of this study include:

- The proposed development is estimated to generate 83 morning peak hour, 73 evening peak hour, and 548 average weekday trips.
- Based on a review of the available crash data and crash rates, patterns are consistent with the geometry and traffic control provided at the study intersection. The proposed project is not expected to change or worsen crash rates. Accordingly, no safety mitigation is recommended per the crash data analysis.
- Preliminary traffic signal warrants are not met at the unsignalized study area intersection under buildout conditions.
- The study intersection is currently operating acceptably per Washington County standards and is projected to continue operating acceptably through the 2023 buildout year of the site. No operational mitigation is required or recommended.
- The construction of the planned five lane cross-section on SW Tualatin-Sherwood Road will not adversely affect future operations at the study intersection.


# Appendix A - Site Information 

Site Plan
Trip Generation Calculations

| gross lot area: | $\begin{gathered} 330,847 \mathrm{sf} \\ 7.60 \text { acres } \end{gathered}$ |
| :---: | :---: |
| NET LOT AREA: | $\begin{gathered} 323,090 \mathrm{sf} \\ 7.42 \text { acres } \end{gathered}$ |
| TOTAL BUILDING AREA: BUILDING A: BUILDING $B$ : | \| 12,525 sf <br> 81,075 <br> $31,050 \mathrm{~s}$ |
| SITE COVERAGE (on NET): | 34.8\% |
| dOCK DOOR RATIO: BUILDING A: BUILDING B | $\begin{aligned} & 1 / 4,054 \mathrm{sf} \\ & 1 / 4,436 \mathrm{sf} \end{aligned}$ |
| PARKING REQUIRED | 93 spaces |
| buliong A: | 67 spaces |
| WAREHOUSE (60\%) at . 3 per 1.000 : | 15 spaces |
| MANUFACTURING (40\%) at 1.6 per 1,000 BUILDING B: | 52 spaces 26 spaces |
| WAREHOUSE (60\%) at . 3 per 1,000: MANUFACTURING (40\%) at 1.6 per 1,000 | 6 spaces <br> 20 space |
| PARKING PROVIDED: total site 92 per 1,000 st | 103 spaces 103 spaces |
| LANDSCAPE REQUIRED: | 48,547 sf ( $15 \%$ ) |
| LANDSCAPE PROVIDED: | TBD |

Calvin J. Coatsworth Architects, PC


TRIP GENERATION CALCULATIONS
Source: Trip Generation Manual, 11th Edition

Land Use: General Light Industrial<br>Land Use Code: 110<br>Land Use Subcategory: All Sites<br>Setting/Location General Urban/Suburban<br>Variable: 1000 SF GFA<br>Trip Type: Vehicle<br>Variable Quantity: 112.6

## AM PEAK HOUR

Trip Rate: 0.74

|  | Enter | Exit | Total |
| :---: | :---: | :---: | :---: |
| Directional Split | $88 \%$ | $12 \%$ |  |
| Trip Ends | 73 | 10 | 83 |

WEEKDAY

Trip Rate: 4.87

|  | Enter | Exit | Total |
| :---: | :---: | :---: | :---: |
| Directional Split | $50 \%$ | $50 \%$ |  |
| Trip Ends | 274 | 274 | 548 |

PM PEAK HOUR
Trip Rate: 0.65

|  | Enter | Exit | Total |
| :---: | :---: | :---: | :---: |
| Directional Split | $14 \%$ | $86 \%$ |  |
| Trip Ends | 10 | 63 | 73 |

SATURDAY

Trip Rate: 0.69

|  | Enter | Exit | Total |
| :---: | :---: | :---: | :---: |
| Directional Split | $50 \%$ | $50 \%$ |  |
| Trip Ends | 39 | 39 | 78 |

## Appendix B - Traffic Data

Turning Movement Counts
In-Process Traffic Data


Note: Total study counts contained in parentheses.

|  | HV\% | PHF |
| :--- | :---: | :---: |
| EB | $16.3 \%$ | 0.92 |
| WB | $10.9 \%$ | 0.88 |
| NB | $13.6 \%$ | 0.61 |
| SB | $0.0 \%$ | 0.00 |
| All | $13.6 \%$ | 0.93 |

Traffic Counts - Motorized Vehicles

| Interval | SW Tualatin Sherwood Rd Eastbound |  |  |  | SW Tualatin Sherwood Rd Westbound |  |  |  | Stie Access <br> Northbound |  |  |  | Stie Access Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 7:00 AM | 0 | 0 | 47 | 1 | 0 | 0 | 54 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 102 | 1,368 |
| 7:05 AM | 0 | 0 | 54 | 0 | 0 | 2 | 50 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 109 | 1,384 |
| 7:10 AM | 0 | 0 | 56 | 0 | 0 | 2 | 55 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 115 | 1,364 |
| 7:15 AM | 0 | 0 | 62 | 0 | 0 | 1 | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 102 | 1,380 |
| 7:20 AM | 0 | 0 | 44 | 0 | 0 | 2 | 46 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 95 | 1,391 |
| 7:25 AM | 0 | 0 | 50 | 2 | 0 | 3 | 69 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 124 | 1,408 |
| 7:30 AM | 0 | 0 | 54 | 1 | 0 | 4 | 62 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 124 | 1,402 |
| 7:35 AM | 0 | 0 | 56 | 4 | 0 | 5 | 60 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 126 | 1,389 |
| 7:40 AM | 0 | 0 | 62 | 1 | 0 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 1,371 |
| 7:45 AM | 0 | 0 | 55 | 1 | 0 | 5 | 79 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 141 | 1,365 |
| 7:50 AM | 0 | 0 | 53 | 2 | 0 | 7 | 71 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 136 | 1,318 |
| 7:55 AM | 0 | 0 | 52 | 4 | 0 | 5 | 32 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 94 | 1,288 |
| 8:00 AM | 0 | 0 | 45 | 1 | 0 | 4 | 65 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 118 | 1,316 |
| 8:05 AM | 0 | 0 | 46 | 1 | 0 | 2 | 39 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 89 |  |
| 8:10 AM | 0 | 0 | 58 | 1 | 0 | 7 | 62 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 131 |  |
| 8:15 AM | 0 | 0 | 54 | 1 | 0 | 1 | 55 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 113 |  |
| 8:20 AM | 0 | 0 | 67 | 2 | 0 | 3 | 36 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 112 |  |
| 8:25 AM | 0 | 0 | 58 | 2 | 0 | 2 | 53 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 118 |  |
| 8:30 AM | 0 | 0 | 62 | 0 | 0 | 1 | 48 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 111 |  |
| 8:35 AM | 0 | 0 | 47 | 0 | 0 | 3 | 57 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 108 |  |
| 8:40 AM | 0 | 0 | 53 | 0 | 0 | 0 | 38 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 94 |  |
| 8:45 AM | 0 | 0 | 43 | 0 | 0 | 1 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 94 |  |
| 8:50 AM | 0 | 0 | 56 | 3 | 0 | 5 | 38 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 106 |  |
| 8:55 AM | 0 | 0 | 54 | 1 | 0 | 1 | 64 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 122 |  |
| Count Total | 0 | 0 | 1,288 | 28 | 0 | 66 | 1,259 | 0 | 0 | 10 | 0 | 33 | 0 | 0 | 0 | 0 | 2,684 |  |
| Peak Hour | 0 | 0 | 652 | 21 | 0 | 46 | 667 | 0 | 0 | 5 | 0 | 17 | 0 | 0 | 0 | 0 | 1,408 |  |

Location: 1 Stie Access \& SW Tualatin Sherwood Rd AM
Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles on Crosswalk

| Interval | Heavy Vehicles |  |  |  |  | Interval Start Time | Bicycles on Roadway |  |  |  |  | Interval Start Time | Pedestrians/Bicycles on Crosswalk |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |
| 7:00 AM | 12 | 0 | 7 | 0 | 19 | 7:00 AM | 0 | 0 | 0 | 0 | 0 | 7:00 AM | 0 | 0 | 0 | 0 | 0 |
| 7:05 AM | 9 | 0 | 3 | 0 | 12 | 7:05 AM | 0 | 0 | 0 | 0 | 0 | 7:05 AM | 0 | 0 | 0 | 0 | 0 |
| 7:10 AM | 9 | 1 | 6 | 0 | 16 | 7:10 AM | 0 | 0 | 0 | 0 | 0 | 7:10 AM | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 12 | 0 | 8 | 0 | 20 | 7:15 AM | 0 | 0 | 0 | 0 | 0 | 7:15 AM | 0 | 0 | 0 | 0 | 0 |
| 7:20 AM | 7 | 0 | 4 | 0 | 11 | 7:20 AM | 0 | 0 | 2 | 0 | 2 | 7:20 AM | 0 | 0 | 0 | 0 | 0 |
| 7:25 AM | 17 | 0 | 7 | 0 | 24 | 7:25 AM | 0 | 0 | 0 | 0 | 0 | 7:25 AM | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 9 | 1 | 3 | 0 | 13 | 7:30 AM | 0 | 0 | 0 | 0 | 0 | 7:30 AM | 0 | 0 | 0 | 0 | 0 |
| 7:35 AM | 11 | 1 | 5 | 0 | 17 | 7:35 AM | 0 | 0 | 1 | 0 | 1 | 7:35 AM | 0 | 0 | 0 | 0 | 0 |
| 7:40 AM | 9 | 0 | 5 | 0 | 14 | 7:40 AM | 0 | 0 | 0 | 0 | 0 | 7:40 AM | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 9 | 0 | 9 | 0 | 18 | 7:45 AM | 0 | 0 | 0 | 0 | 0 | 7:45 AM | 0 | 0 | 0 | 0 | 0 |
| 7:50 AM | 7 | 0 | 8 | 0 | 15 | 7:50 AM | 0 | 0 | 0 | 0 | 0 | 7:50 AM | 0 | 0 | 0 | 0 | 0 |
| 7:55 AM | 5 | 0 | 4 | 0 | 9 | 7:55 AM | 0 | 0 | 0 | 0 | 0 | 7:55 AM | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 8 | 0 | 9 | 0 | 17 | 8:00 AM | 0 | 0 | 0 | 0 | 0 | 8:00 AM | 0 | 0 | 0 | 0 | 0 |
| 8:05 AM | 5 | 0 | 4 | 0 | 9 | 8:05 AM | 0 | 0 | 0 | 0 | 0 | 8:05 AM | 0 | 0 | 0 | 0 | 0 |
| 8:10 AM | 10 | 0 | 10 | 0 | 20 | 8:10 AM | 0 | 0 | 0 | 0 | 0 | 8:10 AM | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 10 | 0 | 6 | 0 | 16 | 8:15 AM | 0 | 0 | 0 | 0 | 0 | 8:15 AM | 0 | 0 | 0 | 0 | 0 |
| 8:20 AM | 10 | 1 | 8 | 0 | 19 | 8:20 AM | 1 | 0 | 0 | 0 | 1 | 8:20 AM | 0 | 0 | 0 | 0 | 0 |
| 8:25 AM | 7 | 1 | 4 | 0 | 12 | 8:25 AM | 0 | 0 | 0 | 0 | 0 | 8:25 AM | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 8 | 0 | 9 | 0 | 17 | 8:30 AM | 0 | 0 | 0 | 0 | 0 | 8:30 AM | 0 | 0 | 0 | 0 | 0 |
| 8:35 AM | 4 | 0 | 10 | 0 | 14 | 8:35 AM | 0 | 0 | 0 | 0 | 0 | 8:35 AM | 0 | 0 | 0 | 0 | 0 |
| 8:40 AM | 7 | 0 | 5 | 0 | 12 | 8:40 AM | 0 | 0 | 0 | 0 | 0 | 8:40 AM | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 10 | 0 | 8 | 0 | 18 | 8:45 AM | 0 | 0 | 0 | 0 | 0 | 8:45 AM | 0 | 0 | 0 | 0 | 0 |
| 8:50 AM | 10 | 0 | 5 | 0 | 15 | 8:50 AM | 0 | 0 | 0 | 0 | 0 | 8:50 AM | 0 | 0 | 0 | 0 | 0 |
| 8:55 AM | 8 | 0 | 5 | 0 | 13 | 8:55 AM | 0 | 0 | 0 | 0 | 0 | 8:55 AM | 0 | 0 | 0 | 0 | 0 |
| Count Total | 213 | 5 | 152 | 0 | 370 | Count Total | 1 | 0 | 3 | 0 | 4 | Count Total | 0 | 0 | 0 | 0 | 0 |
| Peak Hour | 110 | 3 | 78 | 0 | 191 | Peak Hour | 1 | 0 | 1 | 0 | 2 | Peak Hour | 0 | 0 | 0 | 0 | 0 |



Note: Total study counts contained in parentheses.

|  | HV\% | PHF |
| :--- | :---: | :---: |
| EB | $4.1 \%$ | 0.93 |
| WB | $7.3 \%$ | 0.93 |
| NB | $0.0 \%$ | 0.44 |
| SB | $0.0 \%$ | 0.00 |
| All | $5.4 \%$ | 0.95 |

Traffic Counts - Motorized Vehicles

| Interval Start Time | SW Tualatin Sherwood Rd Eastbound |  |  |  | SW Tualatin Sherwood Rd Westbound |  |  |  | Stie Access Northbound |  |  |  | Stie Access Southbound |  |  |  | Total | Rolling Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  |
| 4:00 PM | 0 | 0 | 74 | 0 | 0 | 0 | 44 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 122 | 1,455 |
| 4:05 PM | 0 | 0 | 64 | 0 | 0 | 0 | 56 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 123 | 1,476 |
| 4:10 PM | 0 | 0 | 69 | 1 | 0 | 0 | 69 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 142 | 1,470 |
| 4:15 PM | 0 | 0 | 47 | 1 | 0 | 0 | 59 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 108 | 1,452 |
| 4:20 PM | 0 | 0 | 61 | 0 | 0 | 1 | 52 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 115 | 1,484 |
| 4:25 PM | 0 | 0 | 69 | 0 | 0 | 5 | 55 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 133 | 1,504 |
| 4:30 PM | 0 | 0 | 63 | 0 | 0 | 0 | 67 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 134 | 1,483 |
| 4:35 PM | 0 | 0 | 56 | 1 | 0 | 1 | 38 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 98 | 1,479 |
| 4:40 PM | 0 | 0 | 64 | 0 | 0 | 0 | 54 | 0 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 0 | 124 | 1,507 |
| 4:45 PM | 0 | 0 | 58 | 0 | 0 | 0 | 66 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 125 | 1,528 |
| 4:50 PM | 0 | 0 | 64 | 0 | 0 | 1 | 50 | 0 | 0 | 2 | 0 | 5 | 0 | 0 | 0 | 0 | 122 | 1,515 |
| 4:55 PM | 0 | 0 | 58 | 0 | 0 | 0 | 45 | 0 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 0 | 109 | 1,497 |
| 5:00 PM | 0 | 0 | 78 | 0 | 0 | 0 | 53 | 0 | 0 | 1 | 0 | 11 | 0 | 0 | 0 | 0 | 143 | 1,482 |
| 5:05 PM | 0 | 0 | 54 | 0 | 0 | 0 | 59 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 117 |  |
| 5:10 PM | 0 | 0 | 73 | 0 | 0 | 0 | 44 | 0 | 0 | 2 | 0 | 5 | 0 | 0 | 0 | 0 | 124 |  |
| 5:15 PM | 0 | 0 | 59 | 0 | 0 | 0 | 78 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 140 |  |
| 5:20 PM | 0 | 0 | 78 | 0 | 0 | 0 | 56 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 135 |  |
| 5:25 PM | 0 | 0 | 66 | 0 | 0 | 1 | 45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 112 |  |
| 5:30 PM | 0 | 0 | 58 | 1 | 0 | 0 | 70 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 130 |  |
| 5:35 PM | 0 | 0 | 74 | 0 | 0 | 0 | 50 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 126 |  |
| 5:40 PM | 0 | 0 | 82 | 0 | 0 | 0 | 63 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 145 |  |
| 5:45 PM | 0 | 0 | 67 | 0 | 0 | 0 | 45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 112 |  |
| 5:50 PM | 0 | 0 | 59 | 0 | 0 | 0 | 45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 104 |  |
| 5:55 PM | 0 | 0 | 46 | 1 | 0 | 0 | 46 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 94 |  |
| Count Total | 0 | 0 | 1,541 | 5 | 0 | 9 | 1,309 | 0 | 0 | 17 | 0 | 56 | 0 | 0 | 0 | 0 | 2,937 |  |
| Peak Hour | 0 | 0 | 802 | 1 | 0 | 2 | 679 | 0 | 0 | 7 | 0 | 37 | 0 | 0 | 0 | 0 | 1,528 |  |

Location: 1 Stie Access \& SW Tualatin Sherwood Rd PM
Traffic Counts - Heavy Vehicles, Bicycles on Road, and Pedestrians/Bicycles on Crosswalk

| Interval | Heavy Vehicles |  |  |  |  | Interval Start Time | Bicycles on Roadway |  |  |  |  | Interval Start Time | Pedestrians/Bicycles on Crosswalk |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |  | EB | NB | WB | SB | Total |
| 4:00 PM | 4 | 0 | 3 | 0 | 7 | 4:00 PM | 0 | 0 | 0 | 0 | 0 | 4:00 PM | 0 | 0 | 0 | 0 | 0 |
| 4:05 PM | 1 | 0 | 8 | 0 | 9 | 4:05 PM | 0 | 0 | 0 | 0 | 0 | 4:05 PM | 0 | 0 | 0 | 0 | 0 |
| 4:10 PM | 3 | 0 | 4 | 0 | 7 | 4:10 PM | 0 | 0 | 0 | 0 | 0 | 4:10 PM | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 2 | 0 | 1 | 0 | 3 | 4:15 PM | 0 | 0 | 0 | 0 | 0 | 4:15 PM | 0 | 0 | 0 | 0 | 0 |
| 4:20 PM | 2 | 0 | 3 | 0 | 5 | 4:20 PM | 0 | 0 | 0 | 0 | 0 | 4:20 PM | 0 | 1 | 0 | 0 | 1 |
| 4:25 PM | 3 | 0 | 7 | 0 | 10 | 4:25 PM | 0 | 0 | 0 | 0 | 0 | 4:25 PM | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 5 | 0 | 3 | 0 | 8 | 4:30 PM | 0 | 0 | 0 | 0 | 0 | 4:30 PM | 0 | 1 | 0 | 0 | 1 |
| 4:35 PM | 5 | 0 | 3 | 0 | 8 | 4:35 PM | 0 | 0 | 0 | 0 | 0 | 4:35 PM | 0 | 0 | 0 | 0 | 0 |
| 4:40 PM | 4 | 1 | 7 | 0 | 12 | 4:40 PM | 1 | 0 | 0 | 0 | 1 | 4:40 PM | 0 | 1 | 0 | 0 | 1 |
| 4:45 PM | 0 | 0 | 3 | 0 | 3 | 4:45 PM | 0 | 0 | 0 | 0 | 0 | 4:45 PM | 0 | 0 | 0 | 0 | 0 |
| 4:50 PM | 2 | 0 | 3 | 0 | 5 | 4:50 PM | 0 | 0 | 0 | 0 | 0 | 4:50 PM | 0 | 0 | 0 | 0 | 0 |
| 4:55 PM | 3 | 0 | 1 | 0 | 4 | 4:55 PM | 0 | 0 | 0 | 0 | 0 | 4:55 PM | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 4 | 0 | 4 | 0 | 8 | 5:00 PM | 0 | 0 | 0 | 0 | 0 | 5:00 PM | 0 | 0 | 0 | 0 | 0 |
| 5:05 PM | 4 | 0 | 1 | 0 | 5 | 5:05 PM | 0 | 0 | 0 | 0 | 0 | 5:05 PM | 0 | 0 | 0 | 0 | 0 |
| 5:10 PM | 2 | 0 | 5 | 0 | 7 | 5:10 PM | 0 | 0 | 0 | 0 | 0 | 5:10 PM | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 4 | 0 | 4 | 0 | 8 | 5:15 PM | 0 | 0 | 1 | 0 | 1 | 5:15 PM | 0 | 0 | 0 | 0 | 0 |
| 5:20 PM | 2 | 0 | 5 | 0 | 7 | 5:20 PM | 0 | 0 | 1 | 0 | 1 | 5:20 PM | 0 | 0 | 0 | 0 | 0 |
| 5:25 PM | 5 | 0 | 4 | 0 | 9 | 5:25 PM | 0 | 0 | 0 | 0 | 0 | 5:25 PM | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 3 | 0 | 9 | 0 | 12 | 5:30 PM | 0 | 0 | 0 | 0 | 0 | 5:30 PM | 0 | 0 | 0 | 0 | 0 |
| 5:35 PM | 0 | 0 | 4 | 0 | 4 | 5:35 PM | 0 | 0 | 0 | 0 | 0 | 5:35 PM | 0 | 0 | 0 | 0 | 0 |
| 5:40 PM | 4 | 0 | 7 | 0 | 11 | 5:40 PM | 0 | 0 | 1 | 0 | 1 | 5:40 PM | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 3 | 0 | 3 | 0 | 6 | 5:45 PM | 0 | 0 | 1 | 0 | 1 | 5:45 PM | 0 | 0 | 0 | 0 | 0 |
| 5:50 PM | 2 | 0 | 3 | 0 | 5 | 5:50 PM | 0 | 0 | 0 | 0 | 0 | 5:50 PM | 0 | 0 | 0 | 0 | 0 |
| 5:55 PM | 4 | 0 | 7 | 0 | 11 | 5:55 PM | 0 | 0 | 0 | 0 | 0 | 5:55 PM | 0 | 0 | 0 | 0 | 0 |
| Count Total | 71 | 1 | 102 | 0 | 174 | Count Total | 1 | 0 | 4 | 0 | 5 | Count Total | 0 | 3 | 0 | 0 | 3 |
| Peak Hour | 33 | 0 | 50 | 0 | 83 | Peak Hour | 0 | 0 | 3 | 0 | 3 | Peak Hour | 0 | 0 | 0 | 0 | 0 |



Trip Generation

| Period | In | Out | Total |
| :---: | :---: | :---: | :---: |
| AM | 28 | 4 | 32 |
| PM | 4 | 24 | 28 |
| DAILY | 118 | 118 | 236 |

Trip Distribution


Site Trip Assignment - AM Peak Hour


Site Trip Assignment - PM Peak Hour






## Appendix C - Safety

## Crash Reports

Traffic Signal Warrant Analysis


## Traffic Signal Warrant Analysis



## Appendix D - Operations Analysis

LOS Data Sheets
Synchro Reports

## Level of Service Definitions

Level of service is used to describe the quality of traffic flow. Levels of service A to C are considered good, and rural roads are usually designed for level of service C. Urban streets and signalized intersections are typically designed for level of service D. Level of service E is considered to be the limit of acceptable delay. For unsignalized intersections, level of service E is generally considered acceptable. Here is a more complete description of levels of service:

- Level of service A: Very low delay at intersections, with all traffic signal cycles clearing and no vehicles waiting through more than one signal cycle. On highways, low volume and high speeds, with speeds not restricted by other vehicles.
- Level of service B: Operating speeds beginning to be affected by other traffic; short traffic delays at intersections. Higher average intersection delay than for level of service A resulting from more vehicles stopping.
- Level of service C: Operating speeds and maneuverability closely controlled by other traffic; higher delays at intersections than for level of service B due to a significant number of vehicles stopping. Not all signal cycles clear the waiting vehicles. This is the recommended design standard for rural highways.
- Level of service D: Tolerable operating speeds; long traffic delays occur at intersections. The influence of congestion is noticeable. At traffic signals many vehicles stop, and the proportion of vehicles not stopping declines. The number of signal cycle failures, for which vehicles must wait through more than one signal cycle, are noticeable. This is typically the design level for urban signalized intersections.
- Level of service $E$ : Restricted speeds, very long traffic delays at traffic signals, and traffic volumes near capacity. Flow is unstable so that any interruption, no matter how minor, will cause queues to form and service to deteriorate to level of service F. Traffic signal cycle failures are frequent occurrences. For unsignalized intersections, level of service E or better is generally considered acceptable.
- Level of service F: Extreme delays, resulting in long queues which may interfere with other traffic movements. There may be stoppages of long duration, and speeds may drop to zero. There may be frequent signal cycle failures. Level of service F will typically result when vehicle arrival rates are greater than capacity. It is considered unacceptable by most drivers.

| Level of Service Criteria <br> For Signalized Intersections <br> Control Delay per Vehicle <br> (Seconds) |  |
| :---: | :---: |
| Level of Service (LOS) | $<10$ |
| A | $10-20$ |
| B | $20-35$ |
| C | $35-55$ |
| D | $55-80$ |
| E | $>80$ |
| F |  |

Level of Service Criteria
For Unsignalized Intersections

| Level of Service (LOS) | Control Delay per Vehicle <br> (Seconds) |
| :---: | :---: |
| A | $<10$ |
| B | $10-15$ |
| C | $15-25$ |
| D | $25-35$ |
| E | $35-50$ |
| F | $>50$ |



| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1528 | 713 | 0 | 0 | 724 | 0 |
| Stage 1 | 713 | - | - | - | - | - |
| Stage 2 | 815 | - | - | - | - | - |
| Critical Hdwy | 6.54 | 6.34 | - | - | 4.21 | - |
| Critical Hdwy Stg 1 | 5.54 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.54 | - | - | - | - | - |
| Follow-up Hdwy | 3.626 | 3.426 | - | - | 2.299 | - |
| Pot Cap-1 Maneuver | 121 | 412 | - | - | 839 | - |
| Stage 1 | 465 | - | - | - | - | - |
| Stage 2 | 415 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 114 | 412 | - | - | 839 | - |
| Mov Cap-2 Maneuver | 245 | - | - | - | - | - |
| Stage 1 | 465 | - | - | - | - | - |
| Stage 2 | 391 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | NW |  | NE |  | SW |  |
| HCM Control Delay, s | 15.8 |  | 0 |  | 0.6 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NET | NERNWLn1 |  | SWL | SWT |
| Capacity (veh/h) |  | - | - | 357 | 839 | - |
| HCM Lane V/C Ratio |  | - | - | 0.066 | 0.059 | - |
| HCM Control Delay (s) |  | - | - | 15.8 | 9.6 | - |
| HCM Lane LOS |  | - | - | C | A | - |
| HCM 95th \%tile Q(veh) |  | - | - | 0.2 | 0.2 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement | NWL | NWR | NET | NER | SWL | SWT |
| Lane Configurations | Mr |  | 6 |  | i | 4 |
| Traffic Vol, veh/h | 7 | 37 | 802 | 1 | 2 | 679 |
| Future Vol, veh/h | 7 | 37 | 802 | 1 | 2 | 679 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 200 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 0 | 4 | 4 | 7 | 7 |
| Mvmt Flow | 7 | 39 | 844 | 1 | 2 | 715 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement | NWL | NWR | NET | NER | SWL | SWT |
| Lane Configurations | Mr |  | T |  | F | 4 |
| Traffic Vol, veh/h | 5 | 17 | 713 | 21 | 47 | 842 |
| Future Vol, veh/h | 5 | 17 | 713 | 21 | 47 | 842 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 200 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% | 14 | 14 | 16 | 16 | 11 | 11 |
| Mvmt Flow | 5 | 18 | 767 | 23 | 51 | 905 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement | NWL | NWR | NET | NER | SWL | SWT |
| Lane Configurations | Mr |  | F |  | i | 4 |
| Traffic Vol, veh/h | 7 | 38 | 991 | 1 | 2 | 740 |
| Future Vol, veh/h | 7 | 38 | 991 | 1 | 2 | 740 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 200 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 0 | 4 | 4 | 7 | 7 |
| Mvmt Flow | 7 | 40 | 1043 | 1 | 2 | 779 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1827 | 1044 | 0 | 0 | 1044 | 0 |
| Stage 1 | 1044 | - | - | - | - | - |
| Stage 2 | 783 | - | - | - | - | - |
| Critical Hdwy | 6.4 | 6.2 | - | - | 4.17 | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | - | - | 2.263 | - |
| Pot Cap-1 Maneuver | 85 | 281 | - | - | 647 | - |
| Stage 1 | 342 | - | - | - | - | - |
| Stage 2 | 454 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 85 | 281 | - | - | 647 | - |
| Mov Cap-2 Maneuver | 216 | - | - | - | - | - |
| Stage 1 | 342 | - | - | - | - | - |
| Stage 2 | 453 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | NW |  | NE |  | SW |  |
| HCM Control Delay, s | 21.3 |  | 0 |  | 0 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | N | NERNWLn1 |  | SWL | SWT |
| Capacity (veh/h) |  | - | - | 268 | 647 | - |
| HCM Lane V/C Ratio |  | - | - | 0.177 | 0.003 | - |
| HCM Control Delay (s) |  | - | - | 21.3 | 10.6 | - |
| HCM Lane LOS |  | - | - | C | B | - |
| HCM 95th \%tile Q(veh) |  | - | - | 0.6 | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.9 |  |  |  |  |  |
| Movement | NWL | NWR | NET | NER | SWL | SWT |
| Lane Configurations | r |  | $\uparrow$ |  | T | 4 |
| Traffic Vol, veh/h | 8 | 24 | 713 | 47 | 94 | 842 |
| Future Vol, veh/h | 8 | 24 | 713 | 47 | 94 | 842 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 200 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% | 14 | 14 | 16 | 16 | 11 | 11 |
| Mvmt Flow | 9 | 26 | 767 | 51 | 101 | 905 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |
| Movement | NWL | NWR | NET | NER | SWL | SWT |
| Lane Configurations | Mr |  | $\uparrow$ |  | 1 | 4 |
| Traffic Vol, veh/h | 29 | 79 | 991 | 4 | 9 | 740 |
| Future Vol, veh/h | 29 | 79 | 991 | 4 | 9 | 740 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 200 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 0 | 4 | 4 | 7 | 7 |
| Mvmt Flow | 31 | 83 | 1043 | 4 | 9 | 779 |


| Major/Minor M | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1842 | 1045 | 0 | 0 | 1047 | 0 |
| Stage 1 | 1045 | - | - | - | - | - |
| Stage 2 | 797 | - | - | - | - | - |
| Critical Hdwy | 6.4 | 6.2 | - | - | 4.17 | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | - | - | 2.263 | - |
| Pot Cap-1 Maneuver | 84 | 280 | - | - | 646 | - |
| Stage 1 | 342 | - | - | - | - | - |
| Stage 2 | 447 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 83 | 280 | - | - | 646 | - |
| Mov Cap-2 Maneuver | 213 | - | - | - | - | - |
| Stage 1 | 342 | - | - | - | - | - |
| Stage 2 | 441 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | NW |  | NE |  | SW |  |
| HCM Control Delay, s | 29.5 |  | 0 |  | 0.1 |  |
| HCM LOS | D |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | N | NERNWLn1 |  | SWL | SWT |
| Capacity (veh/h) |  | - | - | 258 | 646 | - |
| HCM Lane V/C Ratio |  | - | - | 0.441 | 0.015 | - |
| HCM Control Delay (s) |  | - | - | 29.5 | 10.7 | - |
| HCM Lane LOS |  | - | - | D | B | - |
| HCM 95th \%tile Q(veh) |  | - | - | 2.1 | 0 | - |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.9 |  |  |  |  |  |
| Movement N | NWL | NWR | NET | NER | SWL | SWT |
| Lane Configurations | * |  | 中 ${ }^{\text {F }}$ |  | ${ }^{7}$ | 44 |
| Traffic Vol, veh/h | 8 | 24 | 713 | 47 | 94 | 842 |
| Future Vol, veh/h | 8 | 24 | 713 | 47 | 94 | 842 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 200 | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% | 14 | 14 | 16 | 16 | 11 | 11 |
| Mvmt Flow | 9 | 26 | 767 | 51 | 101 | 905 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.1 |  |  |  |  |  |
| Movement | NWL | NWR | NET | NER | SWL | SWT |
| Lane Configurations | M |  | 作 |  | 1 | 个4 |
| Traffic Vol, veh/h | 29 | 79 | 991 | 4 | 9 | 740 |
| Future Vol, veh/h | 29 | 79 | 991 | 4 | 9 | 740 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | 200 | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 0 | 4 | 4 | 7 | 7 |
| Mvmt Flow | 31 | 83 | 1043 | 4 | 9 | 779 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1453 | 524 | 0 | 0 | 1047 | 0 |
| Stage 1 | 1045 | - | - | - | - | - |
| Stage 2 | 408 | - | - | - | - | - |
| Critical Hdwy | 6.8 | 6.9 | - | - | 4.24 | - |
| Critical Hdwy Stg 1 | 5.8 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.8 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | - | - | 2.27 | - |
| Pot Cap-1 Maneuver | 123 | 503 | - | - | 631 | - |
| Stage 1 | 304 | - | - | - | - | - |
| Stage 2 | 646 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 121 | 503 | - | - | 631 | - |
| Mov Cap-2 Maneuver | 234 | - | - | - | - | - |
| Stage 1 | 304 | - | - | - | - | - |
| Stage 2 | 637 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | NW |  | NE |  | SW |  |
| HCM Control Delay, s | 18.3 |  | 0 |  | 0.1 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NET | NERNWLn1 |  | SWL | SWT |
| Capacity (veh/h) |  | - | - | 384 | 631 | - |
| HCM Lane V/C Ratio |  | - | - | 0.296 | 0.015 | - |
| HCM Control Delay (s) |  | - | - | 18.3 | 10.8 | - |
| HCM Lane LOS |  | - | - | C | B | - |
| HCM 95th \%tile Q(veh) |  | - | - | 1.2 | 0 | - |


[^0]:    ${ }^{1}$ Institute of Transportation Engineers (ITE), Trip Generation Manual, 114h Edition, 2021.

[^1]:    ${ }^{2}$ https://www.tualatinoregon.gov/projects

[^2]:    ${ }^{3}$ Transportation Research Board, Highway Capacity Manual, $6^{\text {th }}$ Edition, 2016.

