Stormwater Management Facilities

Private Stormwater Report LMC Office Expansion

HDG Job #: CHA081

Prepared For: CJD Holdings, LLC (LMC Construction) 19200 SW Teton Avenue Tualatin, OR 97062

Prepared By:



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'I hereby certify that this Stormwater Management Report for the LMC Office Expansion project has been prepared by me or under my supervision and meets minimum standards of Clean Water Services (CWS) and normal standards of engineering practice.

I hereby acknowledge and agree that the jurisdiction does not and will not assume liability for the sufficiency, suitability, or performance of drainage facilities designed by me.'



Date: March 29, 2019

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Project Overview and Description

Location of Project	19200 SW Teton Ave, Tualatin, OR
Site Area/Acreage Proposed Disturbed Area	5 acres (217,627 sf) 42,687 sf
Nearest Cross Street	SW Teton Ave, Spokane Ct
Property Zoning	General Manufacturing (MG)
Existing Conditions	The site is currently occupied by an office building and associated parking lot.
Proposed Development	The project proposes a single-story addition to the east side of the existing office building, which will include parking lot revisions.
Тах Мар	2S123CB
Tax Lot	200
Flood Zone	Zone AE, Zone X
Permits Required	Building Permit Grading Permit Public Works Permit

Vicinity Map





Methodology

Existing Drainage	Runoff from the existing site is collected via catch basins and piped to the existing wet pond to the south, which is part of a larger sensitive area. Groundwater is very shallow and portions of the parking area spend parts of the year in flood conditions.
Infiltration Results	Infiltration testing was not conducted for this project. However, due to proximity to the existing waterway, assumed shallow groundwater, and location in a flood zone, onsite infiltration will not be possible. In addition, the observable water level of the adjacent waterway (Hedges Creek Marsh), which periodically
PRIVATE Proposed Stormwater Management Techniques	Stormwater will be managed for water quality and quantity using a detention gallery and mechanical filtration system located in the parking area to the north of the proposed building addition.
PUBLIC Proposed Stormwater Management Techniques	Existing curbs and inlets will be protected and improvements will not include additional impervious area. Therefore, no new stormwater management will be required for the public right of way.
Discharge Point	Drainage Way, River, Storm Only Pipe

<u>Analysis</u>

ComputationalHydroCAD models of a SBUH Type 1A Storm were used to calculate the stormwaterMethod Usedmanagement facility sizes for the catchment areas. See attached calculations. Belowis a summary of the results.

Hydrologic Soil Group	B/C/D
Hydrologic Soil Types	Cove clay, Hillsboro loam, Quatama loam

Table 1 – Curve Numbers

Predeveloped Pervious CN	79
Predeveloped Impervious CN	98
Post-Developed Pervious CN	79
Post-Developed Impervious CN	98

Table 2 – Design Storms

WQ Storm	0.36 inches
2-year	2.50 inches
5-year	3.10 inches
10-year	3.45 inches
25-year	3.90 inches
100-year	4.50 inches

Table 3 – Time of Concentration

Predeveloped TOC	5 min
Post-Developed TOC	5 min

The existing stormwater system connects to the wet pond in the sensitive area to the south of the site, which will be fully protected. This system periodically experiences a backwater condition due to the low elevation of the site and its proximity to Hedges Creek Marsh. The total site development area is 42,687 square feet: 7,794 square feet of landscaping, 9,138 square feet of pavement restoration, and 25,842 square feet improved impervious area. The project proposes a detention gallery with orifice flow control and mechanical treatment to meet CWS water quantity and quality requirements for the improved area.

Water quantity: due to the shallow depth of the existing system to the south of the building, a portion of the proposed parking cannot be detained. The proposed detention gallery and orifice flow control manhole are proposed to the north (the highest portion of the site) of the building in order to reduce the instances of a backwater condition that is regularly experienced by the existing stormwater management system to the south. The proposed system will be sized to detain a combined existing and proposed impervious area equal to 23,600 square feet, in order to offset as much of the area that cannot be detained as possible. Stormwater will be detained to match predeveloped runoff rates for the 2, 5, 10, and 25 year storm events, per CWS requirements.

Water quality: All runoff captured by the detention system will also be treated for water quality using a Bayfilter 530 water quality vault. The shallow existing storm system precludes treating a larger area of the site, because of the cover required for the proposed facilities.

Runoff from areas that cannot be detained or treated will be collected via catch basins. All stormwater will then connect to the existing 15" storm line and discharge to the existing wet pond at the south of the site, which was designed to manage the 25-year storm for the full site. Treatment and detention will meet CWS requirements for maintaining existing conditions and protecting the sensitive area.

Catchment/ Facility ID	Source (roof, road, etc.)	Treatment Area (sf)	Ownership (private/ public)	Facility Type/ Function	Facility Size
А	Roof and parking	23,600 sf	Private	Detention gallery & cartridge filter	(21) ADS chambers / (1) bayfilter cartridge
Improved area not managed	Parking	2,242 sf	Private		
Landscape	Landscape	7,744 sf	Private		N/A
Paving Restoration	Parking	9,138 sf	Private		

Table 5 - Flow Rates

	2-Year Storm	5-Year Storm	10-Year Storm	25-Year Storm
Predeveloped	0.08 cfs	0.13 cfs	0.18 cfs	0.24 cfs
Postdeveloped without detention	0.30 cfs	0.37 cfs	0.44 cfs	0.51 cfs
Postdeveloped <u>with</u> detention	0.08 cfs	0.09 cfs	0.11 cfs	0.24 cfs

Engineering Conclusions

The preceding methodologies and calculations presented indicate compliance with the current jurisdictional stormwater management codes and requirements. A summarized breakdown is presented below:

Water Quality	The proposed development will meet the provisions for water quality per CWS storm code.
Water Quantity	The proposed development will meet the provisions for water quantity per CWS storm code.
Downstream / Upstream Impacts	There are no upstream or downstream impacts created by this proposed development.
100 year storm	Since the entire site is located within the floodplian, site runoff will not be conveyed to an alternative system.

Appendix A

Stormwater Facility Details / Exhibits

Utility Plan Predevelopment Impervious Area Catchment Map ADS Detention Gallery Detail Flow Control Manhole Detail Bayfilter 530 Vault Detail



SHE	ET LEGEND
	ONSITE CONCRETE PAVING
	ONSITE ASPHALT PAVING
	PUBLIC ASPHALT PAVING
	PUBLIC CONCRETE PAVING
4. 4	PUBLIC CONCRETE DRIVEWAY
L	SEE LANDSCAPE PLANS
NOT	ES:
1. Al Of	LL WORK IN THE PUBLIC RIGHT F WAY UNDER SEPARATE PERMIT.

SITE DATA

PLANNING DISTRICT DESIGNATION: GENERAL MANUFACTURING (MG)

TOTAL SITE AREA: 214,110 SF

SITE DEVELOPMENT AREA: 42.687 SF

MODIFIED IMPERVIOUS AREA: 23,600 SF

PAVEMENT RESTORATION AREA: 9,138 SF

PROPOSED BUILDING AREA: 13,646 SF

PROPOSED LANDSCAPE AREA: 7.744 SF

PROPOSED PARKING SPACES: STANDARD: 44 ADA: 1

EXISTING PARKING AREA TO BE REMOVED: 6,064 SF

PROPOSED PARKING AREA: 7,336 SF

(503)-232-1987).

GRAPHIC SCALE

1 inch = 20 ft.

STORMWATER NARRATIVE

THE PROPOSED ADDITION TO THE EXISTING BUILDING WILL RESULT IN A NET REDUCTION OF ON-SITE IMPERVIOUS AREA. RUNOFF FROM THE PROPOSED ADDITION, MODIFIED PORTION OF THE PARKING AREA, AND SIDEWALKS WILL BE WANAGED FOR WATER QUANTITY USING A DETENTION SYSTEM AND ORIFICE FLOW-CONTROL MANHIOLE. A CARTRIDGE FILTER SYSTEM WILL BE USED FOR WATER QUALITY, DISCHARGE FROM THE PROPOSED SYSTEM WILL BE DIRECTED TO THE EXISTING WET POND, WHICH CURRENTLY MANAGES THE SITE.

76,071 PRELIMINARY OREGON 14 12, 2053 14 WILLIANS EXPIRES 6-30-2020



Humber Design Group, Inc.

Portland, OR 503.946.6690 hdgpdx.com

> OR TETON BUILDING ADDITION 19200 SW TETON AVE. TUALATIN, LMC CONSTRUCTION ARCHITECTURAL REVIEW APPLICATION

SITE PLAN

PROJECT NO. 18005

3.15.2019

REVISIONS:

C0.50



PREDE\	REDEVELOPED SITE LEGEND						
	SITE DEVELOPMENT AREA: 43,219 SF						
	IMPERVIOUS AREA: 36,599 SF						
	PERVIOUS AREA: 6,088 SF						



LMC OFFICE EXPANSION PREDEVELOPED IMPERVIOUS AREA





LEGEN	LEGEND					
	CATCHMENT A 23,600 SF					
	EXISTING AREA TO BE MANAGED IN CATCHMENT A					
	AREA NOT DETAINED					
	PAVEMENT RESTORATION AREA 9,138 SF					
	LANDSCAPE AREA 7,744 SF					



LMC OFFICE EXPANSION CATCHMENT MAP





ADVANCED DRAINAGE SYSTEMS, INC.

LMC Teton Expansion

Tualatin

STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH SC-740, SC-310, OR APPROVED EQUAL. 1
- CHAMBERS SHALL BE MANUFACTURED FROM VIRGIN POLYPROPYLENE OR POLYETHYLENE RESINS. 2.
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORT PANELS THAT 3. WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- CHAMBERS SHALL MEET ASTM F2922 (POLYETHYLENE) OR ASTM F2418 (POLYPROPYLENE), "STANDARD SPECIFICATION FOR 5 THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- CHAMBERS SHALL BE DESIGNED AND ALLOWABLE LOADS DETERMINED IN ACCORDANCE WITH ASTM F2787, "STANDARD PRACTICE 6 FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS"
- 7 ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. THE CHAMBER MANUFACTURER SHALL SUBMIT THE FOLLOWING UPON REQUEST TO THE SITE DESIGN ENGINEER FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE:
 - A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE SAFETY a. FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY AASHTO FOR THERMOPLASTIC PIPE.
 - A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE LOAD b. FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET. THE 50 YEAR CREEP MODULUS DATA SPECIFIED IN ASTM F2418 OR ASTM F2922 MUST BE USED AS PART OF THE AASHTO STRUCTURAL EVALUATION TO VERIFY LONG-TERM PERFORMANCE.
 - STRUCTURAL CROSS SECTION DETAIL ON WHICH THE STRUCTURAL EVALUATION IS BASED. c.
- CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY. 8

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE SC-310/SC-740 SYSTEM

- STORMTECH SC-310 & SC-740 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A 1. PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- STORMTECH SC-310 & SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/SC-780 CONSTRUCTION 2. GUIDE"
- CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS. 3.

STORMTECH RECOMMENDS 3 BACKFILL METHODS:

- STONESHOOTER LOCATED OFF THE CHAMBER BED.
- BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE. BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- 4. THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS
- JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE. 5
- MAINTAIN MINIMUM 6" (150 mm) SPACING BETWEEN THE CHAMBER ROWS. 6.
- EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 3/4-2" (20-50 mm). 7.
- THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN 8 ENGINEER
- ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE 9 STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT

- 1. STORMTECH SC-310 & SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE"
- THE USE OF CONSTRUCTION EQUIPMENT OVER SC-310 & SC-740 CHAMBERS IS LIMITED: 2 • NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS. • NO RUBBER TIRED LOADERS, DUMP TRUCKS, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- 3. FULL 36" (900 mm) OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.





WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".



ACCEPTABLE FILL MATERIALS: STORMTECH SC-740 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPACTION / I REQUIREME
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPARE PER SITE DESIGN EI PAVED INSTALLATIONS MAY I MATERIAL AND PREPARATION
С	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 18" (450 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMPACTIONS AFTEF MATERIAL OVER THE CHAMB COMPACT ADDITIONAL LAYERS LIFTS TO A MIN. 95% PROCTO WELL GRADED MATERIAL AN DENSITY FOR PROCESSEI MATERIALS. ROLLER GROSS NOT TO EXCEED 12,000 lbs (9 FORCE NOT TO EXCEED 20
В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE, NOMINAL SIZE DISTRIBUTION BETWEEN 3/4-2 INCH (20-50 mm)	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	NO COMPACTION RE
A	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE, NOMINAL SIZE DISTRIBUTION BETWEEN 3/4-2 INCH (20-50 mm)	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	PLATE COMPACT OR ROLL TO SURFACE. 23

PLEASE NOTE:

1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN ANGULAR NO. 4 (AASHTO M43) STONE".

2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 6" (150 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY

3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT CO EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.



NOTES:

- 1. SC-740 CHAMBERS SHALL CONFORM TO THE REQUIREMENTS OF ASTM F2418 "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS", OR ASTM F2922 "STANDARD SPECIFICATION FOR POLYETHYLENE (PE) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 2. SC-740 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 3. "ACCEPTABLE FILL MATERIALS" TABLE ABOVE PROVIDES MATERIAL LOCATIONS, DESCRIPTIONS, GRADATIONS, AND COMPACTION REQUIREMENTS FOR FOUNDATION, EMBEDMENT, AND FILL MATERIALS.
- 4. THE "SITE DESIGN ENGINEER" REFERS TO THE ENGINEER RESPONSIBLE FOR THE DESIGN AND LAYOUT OF THE STORMTECH CHAMBERS FOR THIS PROJECT.
- 5. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
- 6. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 7. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.

		BTONE TO BE DETERMINED ENGINEER 6" (150 mm) MIN		COMPACTOR. OMPACTION	I, CRUSHED,	ACHIEVE A FLAT	,000 lbs (89 kN). :QUIRED.	₹ 12" (300 mm) OF ERS IS REACHED. IN 6" (150 mm) MAX OR DENSITY FOR ID 95% RELATIVE D AGGREGATE VEHICLE WEIGHT 53 kN). DYNAMIC	NGINEER'S PLANS. HAVE STRINGENT I REQUIREMENTS.	DENSITY ENT	
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NTS

INSPECTION & MAINTENANCE

STEP 1) INSPECT ISOLATOR ROW FOR SEDIMENT

A. INSPECTION PORTS (IF PRESENT)

- REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN A.1.
- REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED A.2.
- USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG A.3.
- A.4. LOWER A CAMERA INTO ISOLATOR ROW FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
- IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3. A.5.
- B. ALL ISOLATOR ROWS
- B 1
- REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW THROUGH OUTLET PIPE B.2.
 - i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
 - ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
- B.3. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.

STEP 2) CLEAN OUT ISOLATOR ROW USING THE JETVAC PROCESS

- A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
- APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN Β.
- C. VACUUM STRUCTURE SUMP AS REQUIRED
- REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS. STEP 3)
- INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM. STEP 4)

NOTES

- INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS 1. OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.





CONTACT STORMTECH FOR MORE INFORMATION.

NOTE: ALL DIMENSIONS ARE NOMINAL



MANHOLE W/ DETENTION PIPE



Appendix B

Support Calculations HydroCAD Report



Summary for Subcatchment 3S: Predeveloped

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.08 cfs @ 7.99 hrs, Volume= 1,517 cf, Depth= 0.77"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 2yr Rainfall=2.40"



Summary for Subcatchment 1S: Catchment A

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runon = $0.30 \text{ cis}(Q) (7.81 \text{ hrs}, \text{ volume} = 4.270 \text{ ci}, \text{ Depine} 2.30 \text{ cis}(Q) (7.81 \text{ hrs}, \text{ volume} = 4.270 \text{ ci}, \text{ Depine} 2.30 \text{ cis}(Q) (7.81 \text{ hrs}, \text{ volume} = 4.270 \text{ ci}, \text{ Depine} 2.30 \text{ cis}(Q) (7.81 \text{ hrs}, \text{ volume} = 4.270 \text{ ci}, \text{ Depine} 2.30 \text{ cis}(Q) (7.81 \text{ hrs}, \text{ volume} = 4.270 \text{ ci}, \text{ Depine} 2.30 \text{ cis}(Q) (7.81 \text{ hrs}, \text{ volume} = 4.270 \text{ ci}, \text{ Depine} 2.30 \text{ cis}(Q) (7.81 \text{ hrs}, \text{ volume} = 4.270 \text{ ci}) (7.81 \text{ hrs}) (7.8$	Runoff =	0.30 cfs @	7.81 hrs, Volume=	4,270 cf, Depth= 2.17
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Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 2yr Rainfall=2.40"

	Area (sf)	CN	Description
*	23,600	98	
	23,600		100.00% Impervious Area

Subcatchment 1S: Catchment A



Summary for Pond 2P: (new Pond)

Inflow Are	a =	23,600 sf,	100.00% Impervious,	Inflow Depth = 2.17"	for 2yr event
Inflow	=	0.30 cfs @	7.81 hrs, Volume=	4,270 cf	
Outflow	=	0.08 cfs @	9.17 hrs, Volume=	4,270 cf, Atte	n= 74%, Lag= 81.9 min
Primary	=	0.08 cfs @	9.17 hrs, Volume=	4,270 cf	-
Tertiary	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 125.01' @ 9.17 hrs Surf.Area= 823 sf Storage= 906 cf

Plug-Flow detention time= 114.7 min calculated for 4,270 cf (100% of inflow) Center-of-Mass det. time= 114.5 min (784.7 - 670.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	123.17'	675 cf	15.75'W x 52.28'L x 3.67'H Field A
			3,019 cf Overall - 973 cf Embedded = 2,046 cf x 33.0% Voids
#2A	123.84'	973 cf	ADS_StormTech SC-740 x 21 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 3 rows
		1 648 cf	Total Available Storage

1,648 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Primary	123.17'	1.5" Horiz. Orifice/Grate C= 0.600	
			Limited to weir flow at low heads	
#2	Tertiary	126.75'	6.0" Horiz. Orifice/Grate C= 0.600	
			Limited to weir flow at low heads	

Primary OutFlow Max=0.08 cfs @ 9.17 hrs HW=125.01' (Free Discharge) **1=Orifice/Grate** (Orifice Controls 0.08 cfs @ 6.53 fps)

Tertiary OutFlow Max=0.00 cfs @ 0.00 hrs HW=123.17' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs)

Pond 2P: (new Pond) - Chamber Wizard Field A

Chamber Model = ADS_StormTech SC-740 (ADS StormTech® SC-740)

Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap Row Length Adjustment= +0.44' x 6.45 sf x 3 rows

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

7 Chambers/Row x 7.12' Long +0.44' Row Adjustment = 50.28' Row Length +12.0" End Stone x 2 = 52.28' Base Length 3 Rows x 51.0" Wide + 6.0" Spacing x 2 + 12.0" Side Stone x 2 = 15.75' Base Width 8.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.67' Field Height

21 Chambers x 45.9 cf +0.44' Row Adjustment x 6.45 sf x 3 Rows = 973.2 cf Chamber Storage

3,019.1 cf Field - 973.2 cf Chambers = 2,045.8 cf Stone x 33.0% Voids = 675.1 cf Stone Storage

Chamber Storage + Stone Storage = 1,648.4 cf = 0.038 af Overall Storage Efficiency = 54.6%

21 Chambers 111.8 cy Field 75.8 cy Stone







Pond 2P: (new Pond)

Summary for Subcatchment 3S: Predeveloped

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.13 cfs @ 7.99 hrs, Volume= 2,195 cf, Depth= 1.12"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 5yr Rainfall=2.90"



Summary for Subcatchment 1S: Catchment A

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

1.01011 = 0.0703 (w, 7.01113, V010110 = 0.27001, D0011 = 2.07)	Runoff	=	0.37 cfs @	7.81 hrs, ∖	/olume=	5,248 cf,	Depth=	2.67
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Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 5yr Rainfall=2.90"

	Area (sf)	CN	Description	
*	23,600	98		
	23,600		100.00% Impervious Area	

Subcatchment 1S: Catchment A



Summary for Pond 2P: (new Pond)

Inflow Area	a =	23,600 sf,1	00.00% Impervious,	Inflow Depth = 2.67	" for 5yr event
Inflow	=	0.37 cfs @	7.81 hrs, Volume=	5,248 cf	
Outflow	=	0.09 cfs @	9.30 hrs, Volume=	5,248 cf, Att	en= 75%, Lag= 89.7 min
Primary	=	0.09 cfs @	9.30 hrs, Volume=	5,248 cf	
Tertiary	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 125.59' @ 9.30 hrs Surf.Area= 823 sf Storage= 1,218 cf

Plug-Flow detention time= 145.7 min calculated for 5,248 cf (100% of inflow) Center-of-Mass det. time= 145.5 min (809.7 - 664.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	123.17'	675 cf	15.75'W x 52.28'L x 3.67'H Field A
			3,019 cf Overall - 973 cf Embedded = 2,046 cf x 33.0% Voids
#2A	123.84'	973 cf	ADS_StormTech SC-740 x 21 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 3 rows
		1 648 cf	Total Available Storage

1,648 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Primary	123.17'	1.5" Horiz. Orifice/Grate C= 0.600	
			Limited to weir flow at low heads	
#2	Tertiary	126.75'	6.0" Horiz. Orifice/Grate C= 0.600	
			Limited to weir flow at low heads	

Primary OutFlow Max=0.09 cfs @ 9.30 hrs HW=125.59' (Free Discharge) **1=Orifice/Grate** (Orifice Controls 0.09 cfs @ 7.49 fps)

Tertiary OutFlow Max=0.00 cfs @ 0.00 hrs HW=123.17' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs)

Pond 2P: (new Pond) - Chamber Wizard Field A

Chamber Model = ADS_StormTech SC-740 (ADS StormTech® SC-740)

Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap Row Length Adjustment= +0.44' x 6.45 sf x 3 rows

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

7 Chambers/Row x 7.12' Long +0.44' Row Adjustment = 50.28' Row Length +12.0" End Stone x 2 = 52.28' Base Length 3 Rows x 51.0" Wide + 6.0" Spacing x 2 + 12.0" Side Stone x 2 = 15.75' Base Width 8.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.67' Field Height

21 Chambers x 45.9 cf +0.44' Row Adjustment x 6.45 sf x 3 Rows = 973.2 cf Chamber Storage

3,019.1 cf Field - 973.2 cf Chambers = 2,045.8 cf Stone x 33.0% Voids = 675.1 cf Stone Storage

Chamber Storage + Stone Storage = 1,648.4 cf = 0.038 af Overall Storage Efficiency = 54.6%

21 Chambers 111.8 cy Field 75.8 cy Stone





Pond 2P: (new Pond)



Summary for Subcatchment 3S: Predeveloped

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.18 cfs @ 7.98 hrs, Volume= 2,928 cf, Depth= 1.49"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 10yr Rainfall=3.40"



Summary for Subcatchment 1S: Catchment A

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

	Runoff	=	0.44 cfs @	7.80 hrs, Volum	ne= 6,228 cf, Depth= 3	3.17"
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Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 10yr Rainfall=3.40"

	Area (sf)	CN	Description
*	23,600	98	
	23,600		100.00% Impervious Area

Subcatchment 1S: Catchment A



Summary for Pond 2P: (new Pond)

Inflow Area	a =	23,600 sf,1	00.00% Impervious	Inflow Depth = 3.1	7" for 10yr event
Inflow	=	0.44 cfs @	7.80 hrs, Volume=	6,228 cf	
Outflow	=	0.11 cfs @	9.33 hrs, Volume=	6,228 cf, A	tten= 76%, Lag= 91.7 min
Primary	=	0.11 cfs @	9.33 hrs, Volume=	6,228 cf	
Tertiary	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 126.43' @ 9.33 hrs Surf.Area= 823 sf Storage= 1,538 cf

Plug-Flow detention time= 171.4 min calculated for 6,228 cf (100% of inflow) Center-of-Mass det. time= 171.3 min (831.1 - 659.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	123.17'	675 cf	15.75'W x 52.28'L x 3.67'H Field A
			3,019 cf Overall - 973 cf Embedded = 2,046 cf x 33.0% Voids
#2A	123.84'	973 cf	ADS_StormTech SC-740 x 21 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 3 rows
		1 648 cf	Total Available Storage

1,648 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Primary	123.17'	1.5" Horiz. Orifice/Grate C= 0.600	
			Limited to weir flow at low heads	
#2	Tertiary	126.75'	6.0" Horiz. Orifice/Grate C= 0.600	
			Limited to weir flow at low heads	

Primary OutFlow Max=0.11 cfs @ 9.33 hrs HW=126.43' (Free Discharge) **1=Orifice/Grate** (Orifice Controls 0.11 cfs @ 8.69 fps)

Tertiary OutFlow Max=0.00 cfs @ 0.00 hrs HW=123.17' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs)

Pond 2P: (new Pond) - Chamber Wizard Field A

Chamber Model = ADS_StormTech SC-740 (ADS StormTech® SC-740)

Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap Row Length Adjustment= +0.44' x 6.45 sf x 3 rows

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

7 Chambers/Row x 7.12' Long +0.44' Row Adjustment = 50.28' Row Length +12.0" End Stone x 2 = 52.28' Base Length 3 Rows x 51.0" Wide + 6.0" Spacing x 2 + 12.0" Side Stone x 2 = 15.75' Base Width 8.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.67' Field Height

21 Chambers x 45.9 cf +0.44' Row Adjustment x 6.45 sf x 3 Rows = 973.2 cf Chamber Storage

3,019.1 cf Field - 973.2 cf Chambers = 2,045.8 cf Stone x 33.0% Voids = 675.1 cf Stone Storage

Chamber Storage + Stone Storage = 1,648.4 cf = 0.038 af Overall Storage Efficiency = 54.6%

21 Chambers 111.8 cy Field 75.8 cy Stone





Pond 2P: (new Pond)



Summary for Subcatchment 3S: Predeveloped

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.24 cfs @ 7.98 hrs, Volume= 3,703 cf, Depth= 1.88"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 25yr Rainfall=3.90"



Summary for Subcatchment 1S: Catchment A

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff =	0.51 cfs @	7.80 hrs,	Volume=	7,209 cf,	Depth=	3.67"
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Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 25yr Rainfall=3.90"

	Area (sf)	CN	Description	
*	23,600	98		
	23,600		100.00% Impervious Area	

Subcatchment 1S: Catchment A



Summary for Pond 2P: (new Pond)

Inflow Are	a =	23,600 sf,1	00.00% Impervious,	Inflow Depth = 3.67'	' for 25yr event
Inflow	=	0.51 cfs @	7.80 hrs, Volume=	7,209 cf	
Outflow	=	0.24 cfs @	8.26 hrs, Volume=	7,209 cf, Atte	en= 53%, Lag= 27.3 min
Primary	=	0.11 cfs @	8.26 hrs, Volume=	6,940 cf	
Tertiary	=	0.12 cfs @	8.26 hrs, Volume=	268 cf	

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 126.83' @ 8.26 hrs Surf.Area= 823 sf Storage= 1,647 cf

Plug-Flow detention time= 176.9 min calculated for 7,197 cf (100% of inflow) Center-of-Mass det. time= 177.0 min (833.3 - 656.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	123.17'	675 cf	15.75'W x 52.28'L x 3.67'H Field A
			3,019 cf Overall - 973 cf Embedded = 2,046 cf x 33.0% Voids
#2A	123.84'	973 cf	ADS_StormTech SC-740 x 21 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 3 rows
		1 648 cf	Total Available Storage

1,648 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Primary	123.17'	1.5" Horiz. Orifice/Grate C= 0.600	
	-		Limited to weir flow at low heads	
#2	Tertiary	126.75'	6.0" Horiz. Orifice/Grate C= 0.600	
			Limited to weir flow at low heads	

Primary OutFlow Max=0.11 cfs @ 8.26 hrs HW=126.83' (Free Discharge) —1=Orifice/Grate (Orifice Controls 0.11 cfs @ 9.21 fps)

Tertiary OutFlow Max=0.12 cfs @ 8.26 hrs HW=126.83' (Free Discharge) **2=Orifice/Grate** (Weir Controls 0.12 cfs @ 0.94 fps)

Pond 2P: (new Pond) - Chamber Wizard Field A

Chamber Model = ADS_StormTech SC-740 (ADS StormTech® SC-740)

Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap Row Length Adjustment= +0.44' x 6.45 sf x 3 rows

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

7 Chambers/Row x 7.12' Long +0.44' Row Adjustment = 50.28' Row Length +12.0" End Stone x 2 = 52.28' Base Length 3 Rows x 51.0" Wide + 6.0" Spacing x 2 + 12.0" Side Stone x 2 = 15.75' Base Width 8.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.67' Field Height

21 Chambers x 45.9 cf +0.44' Row Adjustment x 6.45 sf x 3 Rows = 973.2 cf Chamber Storage

3,019.1 cf Field - 973.2 cf Chambers = 2,045.8 cf Stone x 33.0% Voids = 675.1 cf Stone Storage

Chamber Storage + Stone Storage = 1,648.4 cf = 0.038 af Overall Storage Efficiency = 54.6%

21 Chambers 111.8 cy Field 75.8 cy Stone







Pond 2P: (new Pond)

Appendix D

Additional Forms & Associated Reports

Hydrologic Soil Report FEMA Flood Map



Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
14	Cove clay	D	1.2	22.3%
21B	Hillsboro loam, 3 to 7 percent slopes	В	2.5	47.1%
37B	Quatama loam, 3 to 7 percent slopes	С	1.6	30.6%
Totals for Area of Interest			5.4	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



National Flood Hazard Layer FIRMette



Legend

